

Calculation Checksheet

| Project No. <u>18788-003-00</u> Project Title: <u>Mid Barataria Diversion (BA-153)</u> |
|---|
| Deliverable Title: Corrected SPT Number (N ₆₀); Establish Soil Properties for Granular Soil |
| Calculations Description: The standard penetration number is a function of the input |
| driving energy and its dissipation around the sampler into the surrounding soil. The |
| variations of correction to borehole diameter, sampler and rod length are based on |
| recommendations by Seed et al. (1985) and Skempton (1986). The hammer efficiency for |
| the SPT hammer on each of the drill rigs used for the above project were taken from the |
| respective hammer calibration reports. Supporting information is attached. |
| Soil properties for granular soil were established for the above project based on various |
| references attached. |
| Originator: VT Checked by: 1. Clay Date: 11/11/2013 |
| Checking method (describe): |
| |
| Comments: |
| |
| |
| |
| |
| Attach checksheets, numbered consecutively. |

Soil Properties for Mid Barataria Diversion Project (BA-153)

| Soil Type/Relative Density | Unit Weight (pcf) | Cohesion (psf) | Effective Friction Angle (deg) | SPT Blows Corrected (N ₆₀) |
|--|----------------------|-------------------|-----------------------------------|--|
| | | | | |
| Silt | | | | |
| Very Loose | 113 | 200 | 8 | 0-4 |
| Loose | 115 | 200 | 10 | 5-10 |
| (USACE) Medium Dense | 117 | 200 | 15 | 11-30 |
| Dense | 122 | 200 | 20 | 31-50 |
| Very Dense | 125 | 200 | 25 | 51+ |
| Silty (>12%) Sand(>50%)/ Clayey(>12%) Sand (>50%) | | | | |
| Very Loose | 118 | 0 | 25 | 0-4 |
| Loose | 120 | 0 | 28 | 5-10 |
| (USACE for SM) Medium Dense | 122 | 0 | 30 | 11-30 |
| Dense | 125 | 0 | 33 | 31-50 |
| Very Dense | 128 | 0 | 35 | 51+ |
| Poorly Graded Sand | | | | |
| Very Loose | 122 | 0 | 28 | 0-4 |
| Loose | 122 | 0 | 30 | 5-10 |
| (USACE) Medium Dense | 122 | 0 | 33 | 11-30 |
| Dense | 128 | 0 | 39 | 31-50 |
| Very Dense | 130 | 0 | 41 | 51+ |
| | | | | |

Clay properties are based on lab testing performed for the project

Soil Parameters for S-Case: Silt: Cohesion=0 psf, phi=28 Clay: Cohesion=0 psf, phi=23

| Prepared By: | Reviewed By: |
|----------------------|-----------------------|
| Name: Venu Tammineni | Name: Charlie Eustis |
| Date: 11/08/2013 | Date: <u>11/08/13</u> |

= N 14 h B 2 5 2 12

Where

N60 = Standard penetration number, corrected for held N = measured penetration number conditions

14 = hammer efficiency (1.) From hammer calibration

MR = correction for borehole diameter = 1.0 for 4" borchole = 1.05 for 6" borchole

Ms = Sempler correction = 1.0

1/2 = Correction for rod length >30'=1.0 12'-70'=0.85 20'-30'=0.95 6'-12'=0.75

- Variations of 2H, 2B, 25 and 2R, based on recommendations by seed of al. (1985) and 5 kempton (1986)

- Harmmer efficiency was measured for each drill rig (Appendices & through & - Geotechnical Data Report)

Equation and Factors Fizim;

Principals of Foundation Engineering SE, Braja M. Das 2004



US Army Corps of Engineers

ENGINEERING AND DESIGN

Design of Sheet Pile Walls



| Table 3-1 | | | | |
|---------------------------------|--------|------|-------|--|
| Granular Soil Properties | (after | Tena | 1962) | |

| | Relative | SPT N | Angle of Internal | Unit Weight | |
|-------------|----------------|-------------------|----------------------|-------------|-----------------|
| Compactness | Density (%) | (blows per ft) | Friction (deg) | Moist (pcf) | Submerged (pcf) |
| Very Loose | 0-15 | 0-4 | <28 | <100 | <60 |
| Loose | 16-35 | 5-10 | 28-30 | 95-125 | 55-65 |
| Medium | 36-65 | 11-30 | 31-36 | 110-130 | 60-70 |
| Dense | 66-85 | 31-50 | 37-41 | 110-140 | 65-85 |
| Very Dense | 86-100 | >51 | >41 | >130 | >75 |

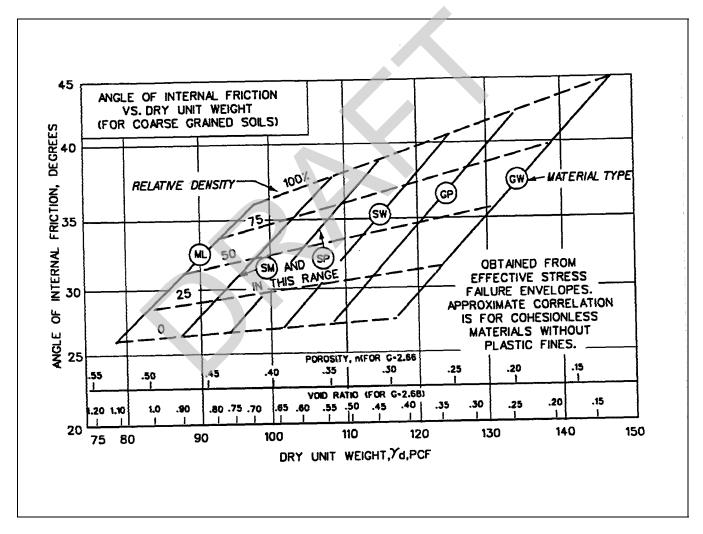


Figure 3-1. Cohesionless Soil Properties (after U.S. Department of the Navy 1971)

Hurricane and Storm Damage Risk Reduction System Design Guidelines



New Orleans District Engineering Division With Revisions through June 2012



UPDATED 14 JUN 12

Table 3.3 Typical Values for Silts, Sands, and Riprap

| Soil Type | Unit Weight (pcf) | Cohesion (psf) | Friction Angle (degree) |
|--------------------|-------------------|-------------------|-------------------------|
| Silt | 117 | 200 | 15 |
| Silty Sand | 122 | 0 | 30 |
| Poorly graded sand | 122 | 0 | 33 |
| Riprap | 132 | 0 | 40 |

Notes:

- 1. Weight of riprap may vary based on the filling of the riprap voids over time.
- 2. Undrained soil parameters for S-Case are:
 - i. Silt Cohesion = 0 psf, phi = 28
 - ii. Clay Cohesion = 0 psf, phi = 23
- 3. Engineering judgment or laboratory test data (if available) should be used in determining soil properties of clayey silts, clayey sands, and sandy silts if they exist in the foundation.

F. Reserved.

G. At pipeline crossings, the allowable FOS shall be 1.5 for the gross section for a distance of 150 ft on either side of the C/L of the pipeline or an appropriate distance determined by engineering assessment. This analysis should be performed with flood side water at the SWL.

3.1.3 Seepage Analysis

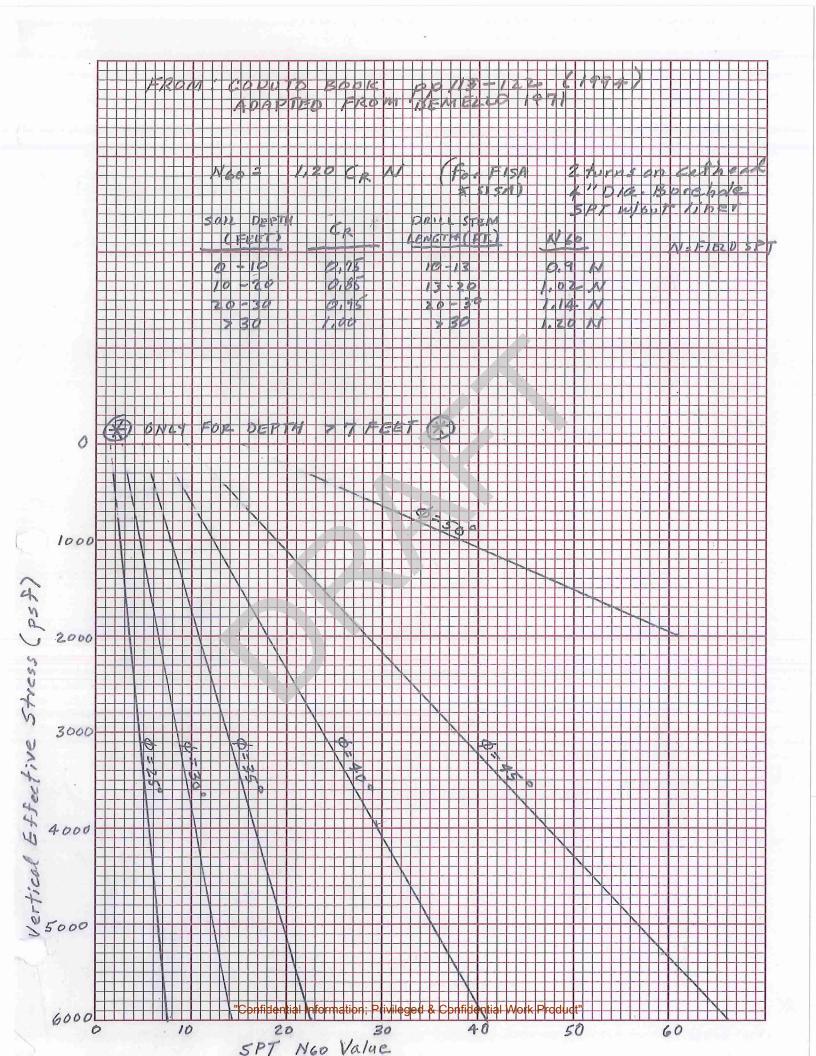
3.1.3.1 Definitions

Stage or Water Surface Elevation (WSE) – the height of water against a levee or floodwall. Water height is measured as the vertical distance above or below a local or national elevation datum.

Design Water Surface Elevation (DWSE) – the stage or water level to be used in deterministic analyses such as the geotechnical, structural stability, and seepage analyses. For the HSDRRS, the DWSE is found from the AWSE and its associated uncertainty at the selected confidence limit, where uncertainty is represented by normal distribution, and the confidence limit is 90%:

AWSE = best fit for 50% confidence level

DWSE = 90% confidence level













Job No. 1332046-1



engineers, inc.

Report on:

SPT Energy Measurements
Diedrich D50: Track Mounted Drill Rig
Automatic Hammer Calibration: SN# 268
Baton Rouge, Louisiana

Prepared for:

Southern Earth Sciences, Inc.By Jon Honeycutt & Brian Mondello, P.E.

December 3rd, 2013

"Confidential Information: Privileged & Confidential Work Produc



December 3, 2013

Mr. Mike Juneau, P.E. Southern Earth Sciences, Inc. 11638 Sun Belt Court Baton Rouge, Louisiana

Re: SPT Energy Measurements

Diedrich D50 - Automatic Hammer Calibration

GRL Job No. 1332046-1

Mr. Juneau:

This report presents the results of Standard Penetration Test (SPT) dynamic energy measurements performed December 2, 2013 on one (1) SPT sampling system at the referenced project site. The objective of the testing was to obtain the SPT energy measurements for the purpose of documenting the hammer energy transfer efficiency. A PDA system, Model PAX, was used to acquire and process the dynamic test data obtained through an instrumented drill rod section. All energy measuring and processing equipment are manufactured by Pile Dynamics, Inc. General information regarding the testing equipment and procedures is provided in Appendix A. Testing results are presented in Appendix B.

Drill Rig and SPT Hammer Details

Testing was conducted on a SPT drilling rig/hammer system that was identified to us as a Diedrich D50 track-mounted drill rig. The SPT system utilized a Diedrich automatic hammer system. The hammer reportedly consisted of a 0.14 kip hammer weight with a 30-inch (2.5 feet) drop height, corresponding to a potential energy value of 0.35 kip-ft.

Type AW-J drilling rods were used during testing. The SPT energy measurements were made using an approximately 3-foot long instrumented AW-J type rod segment inserted into the drill string immediately below the anvil of the hammer. The cross-sectional area of the AW-J instrumented rod segment is 1.16 in².

Southern Earth Sciences, Inc. SPT Energy Measurements GRL Job No. 1332046-1 Page 2 of 4

DYNAMIC TESTING FIELD DETAILS

Instrumentation

A PDA system was used to obtain and process dynamic measurements of strain and acceleration taken on the instrumented AW-J rod segment located between the hammer and drill string. Strain and acceleration signals were conditioned and converted to forces and velocities by the PDA. For each hammer blow, the PDA provided the following quantities: maximum force (FMX), maximum velocity (VMX), maximum displacement (DMX), maximum transferred energy (EFV), energy transfer ratio (ETR), and hammer blow rate per minute (BPM). Force and velocity records from the PDA were also viewed on a graphic LCD screen to evaluate data quality.

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Test Sequence

Dynamic measurements were made at a test boring location at the referenced project site. SPT sampling and dynamic measurements were conducted at starting depths ranging from 25 and 35 ft. Energy measurements were obtained over three 6-inch increments for each sample depth. Based on ASTM 4633-10 requirements, only energy measurements obtained over the last one-foot of driving were used for hammer efficiency evaluation. The reported SPT N-values ranged between 12 and 15 blows/foot.

DYNAMIC TESTING ANALYSIS AND RESULTS

Complete testing and analyses results are presented in Appendix B. A summary of the testing results for the test boring are provided in Table1. PDIPLOT summaries of test records obtained under typical hammer blows from each test sequence are also included.

Energy Transfer Measurements

The PDA interprets the measured dynamic data according to the Case Method equations. Appendix B contains PDA output quantities plotted and printed as functions of hammer blow number for each depth sequence.

The maximum transferred energy (EFV) was calculated by integrating the product of the force and velocity records over the time duration of each test record as follows:

$$EFV = \int F(t)V(t)dt$$

Where, F(t) and V(t) are the time records of force and velocity, respectively.

The Energy Transfer Ratio (ETR) was calculated as:

Where, PE is the potential energy = 140 lbs x 30 inches = 0.14 kips x 2.5 ft = 0.350 kip-ft.

Summary of Testing Results

"Diedrich D50" - Automatic Hammer - AW-J Rod

EFV values ranged between 0.290 and 0.315 kip-ft with an overall average of 0.299 kip-ft and a standard deviation of 0.014 kip-ft. The corresponding ETR values ranged from 82% to 90%, with an overall average of 85% and a standard deviation of 4.0%. The hammer blow rate ranged from 50 to 51 blows/minute (BPM) with an overall average of 50 BPM and standard deviation of 0.3 BPM.

We appreciate the opportunity to be of assistance to you on this project. Please do not hesitate to contact us if you have any questions regarding this report, or if we may be of further service.

Very truly yours, GRL Engineers, Inc.

Jonathan Honeycutt

GRL Engineer

Enclosed: Appendices A and B

Brian Mondello, P.E.

GRL Engineer



SPT Hammer Calibration – Diedrich D50 Automatic, SN# 268

Table 1: Summary of Results

Project: Southern Earth Science | GRL Job No. 1332046-1

Rig: Diedrich D50, Serial No. 268 **Hammer Type:** Automatic

| Boring I.D. | Test | Rod 1 | Sample ² | Sample | Reported | Reported | Blows | Average | Avg. Max. | Average | Average | Average ³ |
|-------------|-------------|--------|---------------------|--------|------------|--------------|---------------|---------|-------------|----------|-------------|----------------------|
| | Date | Length | Depths | No. | blows per | SPT blow | Analyzed | Hammer | Compressive | Maximum | Transferred | Transfer |
| | | | | | 6 inches | count | | Rate | Force | Velocity | Energy | Ratio |
| | | (ft) | (ft) | | (blows/6") | (blows/foot) | | (bpm) | (kips) | (ft/sec) | (lb-ft) | (%) |
| Boring # 1 | 02-Dec-2013 | 28.9 | 25-26.5 | SS1 | 4-5-7 | 12 | 12 | 50.7 | 28.0 | 20.0 | 291 | 83.2 |
| | | 36.9 | 30-31.5 | SS2 | 5-6-6 | 12 | 12 | 50.2 | 32.0 | 23.3 | 315 | 90.0 |
| | | 41.9 | 35-36.5 | SS3 | 6-8-7 | 15 | 12 | 50.1 | 29.0 | 20.8 | 290 | 82.8 |
| | | | | | | | | | | | | |
| | | | | | | | Average: | 50.3 | 29.7 | 21.4 | 299 | 85.3 |
| | | | | | | Standa | rd Deviation: | 0.3 | 2.1 | 1.7 | 14.2 | 4.0 |

Notes:

- 1 Total rod length, including sampler, below gages
- 2 Depths measured from below reference elevation
- 3 Ratio of average transferred energy (EFV) to theoretical potential energy of 350 ft-lbs (140 lbs x 30 inch drop)

APPENDIX A AN INTRODUCTION INTO SPT DYNAMIC PILE TESTING

The following has been written by GRL Engineers, Inc. and may only be copied with its written permission.

1. BACKGROUND

The Standard Penetration Test is frequently conducted as an in-situ assessment of soil strength. This test requires that a 140 lb weight is dropped 30 inches onto a drive rod at whose bottom a sampler is usually installed. The sampler is driven for 18 inches; the number of blows required for the last 12 inches of driving is the so-called N-value. The N-value may be used as a strength indicator for foundation design or as a means of assessing the liquefaction potential of soils.

Obviously, the SPT hammer efficiency is an important consideration when using the N-values for design purposes. Measurements have indicated that the energy in the drive rod is sometimes only 30% and and may reach 90% of the potential or rated energy of the SPT hammer (E-rated = 0.35 kip-ft or 0.475 kJ). The type of hammer used to drive the rod is the main reason for these variations. On the average, the energy in the drive rod is 60% of the standard rated energy.

Because of the variability of energy, methods based on N-values are considered unreliable. However, measurements during SPT testing using the Case Method can be done on a routine basis and these measurements yield the transferred energy values. With measured energy, EMX, known, an adjustment of the measured N-value, N_m, can be made as follows.

$$N_{60} = N_{m} [E_{m} / (0.6E_{r})]$$
 (1)

Thus, if the measured energy value is equal to the normally expected transferred energy of 60% of Erated then the adjusted and measured N-values are identical. On the other hand, if the measured energy is only 30% then the adjusted blow count will be reduced by 50%.

2. DYNAMIC TESTING AND ANALYSIS METHODS APPLIED TO SPT

The Case Method of dynamic pile testing, named after the Case Institute of Technology where it was developed between 1964 and 1975, requires that a substantial ram mass (e.g. a pile driving hammer) impacts the pile top such that the pile undergoes at least a small permanent set. Thus, the method is also referred to as a "High Strain Method". The Case Method requires dynamic measurements on the pile or shaft under the ram impact and then a calculation of various quantities. Conveniently, for SPT applications, the measurements and analyses are done by a single piece of equipment: the SPT Analyzer. The Pile Driving Analyzer® (PDA) is also suitable to perform these measurements and data processing.

A related analysis method is the "Wave Equation Analysis" which calculates a relationship between bearing capacity, pile stresses, transferred energy and field blow count. The GRLWEAPTM program performs this analysis and provides a complete set of helpful information and input data. This program can be used very effectively to simulate the SPT driving process.

3. MEASUREMENTS

GRL uses equipment manufactured by Pile Dynamics, Inc. The system includes either an SPT-Analyzer™ (SPTA) or a Pile Driving Analyzer® (PDA), an instrumented rod section and two accelerometers. SPT energy testing is very closely related to and borrows procedures from dynamic pile testing. Those interested in the basis of the SPT energy testing method may obtain extensive literature on dynamic pile testing from GRL Engineers, Inc.

3.1 SPT Analyzer or Pile Driving Analyzer

The basis for the results calculated by the SPTA or PDA are strain and acceleration measured in an instrumented rod section. These signals are converted to rod top force, F(t), and rod top velocity, v(t). The SPTA or PDA conditions, calibrates and displays these signals and immediately computes average pile force and velocity thereby eliminating bending effects. The product of these two

measurements is then integrated over time which yields the energy transferred to the instrumented section as a function of time (see Section 4.1).

For convenience and accuracy, strain measurements are usually taken on an instrumented section of SPT drive rod. Ideally, the section properties of the instrumented rod and those of the drive rod are the same, however, using subs, other sections can also be utilized.

For the instrumented section, PDI provides a force calibration in such a way that the output of the instrumented rod is directly calculated without the need for an accurate elastic modulus or cross sectional area of the rod section.

The acceleration measurements are often demanding in the SPT environment, because of high frequency and high acceleration motion components. An experienced measurement engineer, therefore, has to evaluate the quality of this data before final conclusions are drawn from the numerical results calculated by SPTA or PDA.

SPTA or PDA records are taken while the standard N-value is acquired in the conventional manner. This then allows a direct correlation between N-value and average transferred energy.

3.2 HPA

The SPT hammer's ram velocity may be directly obtained using radar technology in the Hammer Performance Analyzer™. The impact velocity results can be automatically processed with a PC or recorded on a strip chart. HPA measurements yield a hammer kinetic energy, but not the energy transferred to the drive rod.

4 RECORD EVALUATION BY SPTA OR PDA

4.1 HAMMER PERFORMANCE

The PDA calculates the energy transferred to the pile top from:

$$E(t) = \int_{0}^{t} F(\tau)v(\tau) d\tau$$
 (2)

The maximum of the E(t) curve is often called **ENTHRU** or **EMX**; it is the most important quantity for an overall evaluation of the performance of a hammer

and driving system. **EMX** allows for a classification of the hammer's performance when presented as, e_T , the rated transfer efficiency, also called energy transfer ratio (**ETR**) or global efficiency.

$$e_{T} = EMX/E_{R} \tag{3}$$

where $E_{\rm R}$ is the hammer manufacturer's rated energy value or 0.35 kip-ft (0.475 kJ) in the case of the SPT hammer.

Often in the SPT literature one finds also reference to the EF2 energy. This evaluation is based on assumed proportionality between force and velocity (see also Section 5):

$$v(t) = F(t) / Z \tag{4}$$

where Z = EA/c is the pile impedance, E is the elastic modulus, A is the cross sectional area and c is the speed of the stress wave in the pile material..

Combining equations 2 and 4 leads to

$$\mathsf{EF}(\mathsf{t}) = \int_{\mathsf{O}} \mathsf{t} \, \mathsf{F}(\mathsf{T})^2 / \, \mathsf{Z} \, \mathsf{d}\mathsf{T} \tag{5}$$

The EF2 transferred energy value is the EF-value at the time t = 2L/c, where L is the drive rod length and c is the stress wave speed in steel (16,800 ft/s or 5,124 m/s). Since the force is easier to measure than both force and velocity, Equation 5 is preferred by some test engineers. However, the EF method is fraught with errors and certain correction factors have to be applied to make it approximately correct. Among the error sources are the following:

- Proportionality is often violated prior to time 2L/c. The proportionality between force and velocity in a downward traveling wave only holds if the wave does not encounter a disturbance prior to reflecting off the pile toe. Such disturbances include a change in cross sectional area, an open or loose splice or joint, or resistance along the shaft.
- Using only one force measurement precludes a data quality check based on the proportionality between force and velocity. Thus, a force measurement that is for some reason in error may not be detectable, which will lead to errors in the EF2 value. Data quality checks will be discussed further in Section 5.

The use if EF2 is therefore not recommended but it is often included in result presentations for the sake of completeness.

4.2 STRESSES

During SPT monitoring, it is also of interest to monitor compressive stresses at both the top of the drive rod and at its bottom.

At the pile top (location of sensors) the maximum compression stress averaged over the rod's cross section, **CSX**, is directly obtained from the measurements. Note that this stress value refers to the instrumented section. If the rod has a different cross sectional area then the stress in the rod will be different from CSX.

The SPTA or PDA can also calculate, in an approximate manner, the force at the rod bottom, **CFB**. To obtain the corresponding stress, this force value should be divided by the appropriate cross sectional area, e.g. by the rod area just above the sampler or by the sampler area itself. Of course, non-uniform stress components as they might occur at the sampler tip due to a sloping rock are not considered in this calculation.

5. DATA QUALITY CHECKS

Quality data is the first and foremost requirement for accurate dynamic testing results. It is therefore important that the measurement engineer performing SPTA or PDA tests has the experience necessary to recognize measurement problems and take appropriate corrective action should problems develop. Fortunately, dynamic pile testing allows for certain data quality checks because two independent measurements are taken that have to conform to the so-called proportionality relationship.

As long as there is only a wave traveling in one direction, as is the case during impact when only a downward traveling wave exists in the rod, force and velocity measured at its top are proportional

$$F = V Z \tag{5}$$

where Z is again the pile impedance, Z = EA/c. This relationship can also be expressed in terms of stress

$$\sigma = F/A = v (E/c) \tag{6}$$

or strain

$$\varepsilon = \sigma/E = v/c$$
 (7)

This means that the early portion of strain times wave speed must be equal to the velocity unless the proportionality is affected by high friction near the pile top or by a pile cross sectional change not far below the sensors. Checking the proportionality is an excellent means of assuring meaningful measurements but is only truly meaningful for perfectly uniform rods. Open or loose splices, for example, will lead to a non-proportionality. For SPT rods it is fortunate that usually no soil resistance acts along the shaft and for that reason, proportionality can exist until the stress wave returns from sampler top or rod bottom unless connectors are not sufficiently tightened or have a significant mass.

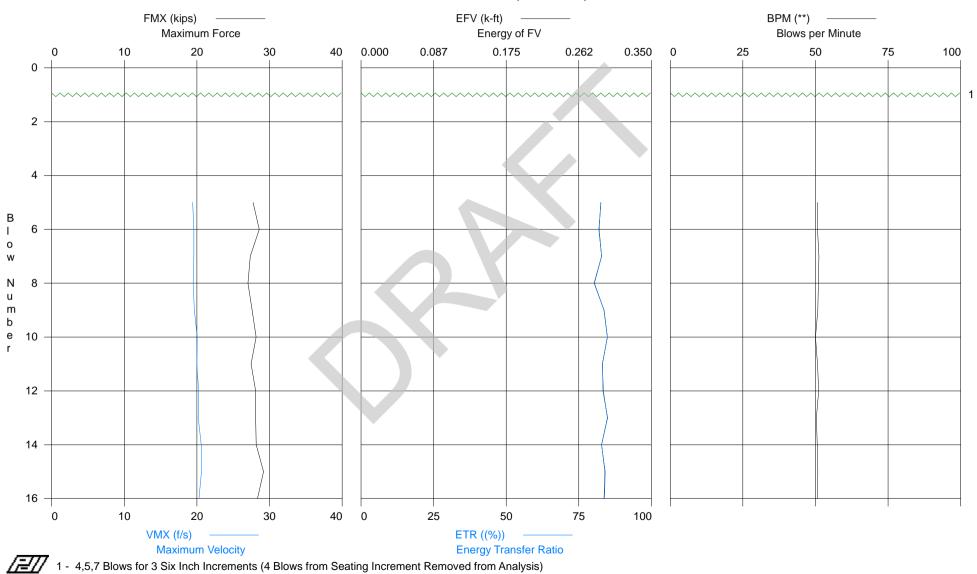
Velocity data quality can also be checked by looking at the final displacement, DFN, which is calculated from the acceleration by double integration. If the calculated final displacement is much higher or lower than indicated by the N-value, the accelerometer attachment may be loose or the sensor may be faulty. If major drift in the velocity is observed, the EMX value may be in error, even though proportionality from impact to time 2L/c exists. In this case, it may be useful to evaluate the energy transferred to the drill rod at time 2L/c, which is calculated by the PDA or SPTA as the E2E quantity.

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Test date: 2-Dec-2013

PDIPLOT Ver. 2012.2 - Printed: 3-Dec-2013

Southern Earth Science - SPT Hammer Calibration - SS1 @ 25 FT Diedrich D50 Automatic, SN#268, AWJ



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| South OP: N | | Science - SF | PT Hamme | er Calibration | on - SS1 (| 25 FT | Diedrich | D50 Autom Tes | atic, SN#2 t date: 2-D | - |
|----------------|-------------|--------------|----------|----------------|------------|----------|------------|------------------|---------------------------|-----------|
| AR: | 1.16 in/ | ^2 | | | | | | | | 492 k/ft3 |
| LE: | 28.90 ft | | | | | | | | EM: 30, | |
| WS: 1 | 6,807.9 f/s | | | | | | | | JC: 0 | 0.00 |
| FMX: | Maximum | Force | | | | | | BPM: Blo | ws per Mir | nute |
| VMX: | Maximum | Velocity | | | | | | | ergy of FV | |
| VT1: | Velocity a | t Time 1 | | | | | | EFV: End | ergy of FV | |
| DMX: | Maximum | Displaceme | ent | | | | | ETR: En | ergy Trans | fer Ratio |
| DFN: | Final Disp | lacement | | | | | | | | |
| BL# | depth | FMX | VMX | VT1 | DMX | DFN | BPM | E2E | EFV | ETR |
| | ft | kips | f/s | f/s | in | in | ** | k-ft | k-ft | (%) |
| 5 | 0.00 | 28 | 19.4 | 19.4 | 1.12 | 0.56 | 50.6 | 0.271 | 0.289 | 82.64 |
| 6 | 0.00 | 29 | 19.6 | 19.6 | 1.14 | 0.61 | 50.7 | 0.272 | 0.287 | 81.90 |
| 7 | 0.00 | 27 | 19.6 | 19.6 | 1.04 | 0.26 | 51.2 | 0.274 | 0.290 | 82.87 |
| 8 | 0.00 | 27 | 19.5 | 19.5 | 0.97 | 0.13 | 51.0 | 0.270 | 0.281 | 80.41 |
| 9 | 0.00 | 28 | 19.6 | 19.6 | 0.97 | 0.62 | 50.8 | 0.272 | 0.293 | 83.65 |
| 10 | 0.00 | 28 | 20.0 | 20.0 | 0.95 | 0.37 | 50.0 | 0.278 | 0.297 | 84.84 |
| 11 | 0.00 | 27 | 20.0 | 20.0 | 0.87 | -0.08 | 50.7 | 0.278 | 0.291 | 83.17 |
| 12 | 0.00 | 28 | 20.3 | 20.3 | 0.82 | 0.16 | 51.1 | 0.274 | 0.292 | 83.31 |
| 13 | 0.00 | 28 | 20.2 | 20.2 | 0.83 | 0.29 | 50.3 | 0.275 | 0.297 | 84.95 |
| 14 | 0.00 | 28 | 20.6 | 20.6 | 0.76 | 0.00 | 50.6 | 0.276 | 0.290 | 82.81 |
| 15 | 0.00 | 29 | 20.6 | 20.6 | 0.73 | 0.11 | 50.8 | 0.276 | 0.294 | 84.11 |
| 16 | 0.00 | 28 | 20.3 | 20.3 | 0.72 | 0.01 | 50.7 | 0.273 | 0.293 | 83.85 |
| | Average | 28 | 20.0 | 20.0 | 0.91 | 0.25 | 50.7 | 0.274 | 0.291 | 83.21 |
| | | | | Total | number of | blows ar | nalyzed: 1 | 2 | | |

BL# depth (ft) Comments

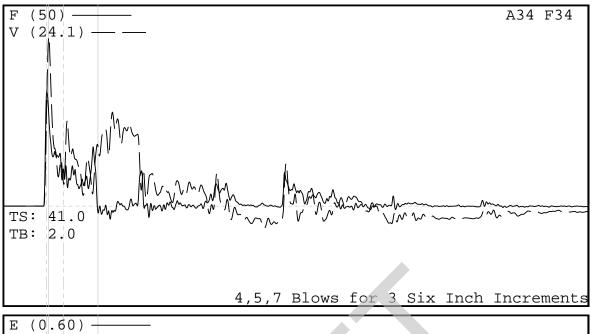
1 0.00 4,5,7 Blows for 3 Six Inch Increments (4 Blows from Seating Increment Removed from Analysis

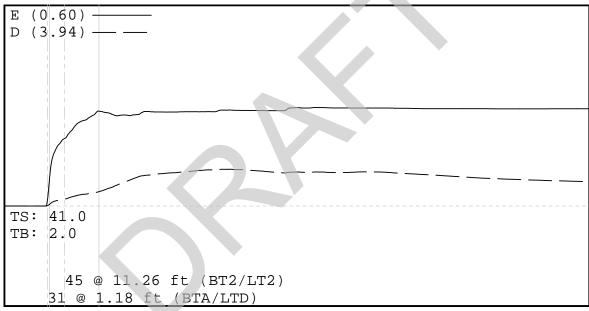
Time Summary

Drive 18 seconds 9:25:45 AM - 9:26:03 AM (12/2/2013) BN 1 - 16

Southern Earth Science - SPT Hammer Calibration

SS1 @ 25 FT





<u>Project Information</u> <u>Quantity Results</u>
PROJECT: Southern Earth Science - SPT Hamm@FMXalib28:ikips

PROJECT: Southern Earth Science - SPT Hammi-MX3lib28:kips
PILE NAME: SS1 @ 25 FT VMX 20.3 f/s
DESCR: Diedrich D50 Automatic, SN#268, AWJVT1 20.3 f/s
OPERATOR: M.J. DMX 0.72 in
FILE: SS1 25 FT.W01 DFN 0.01 in
12/2/2013 9:26:03 AM BPM 50.7 bpm
Blow Number 16 E2E 0.27 k-ft
EFV 0.29 k-ft
Pile Properties ETR 83.8 (%)

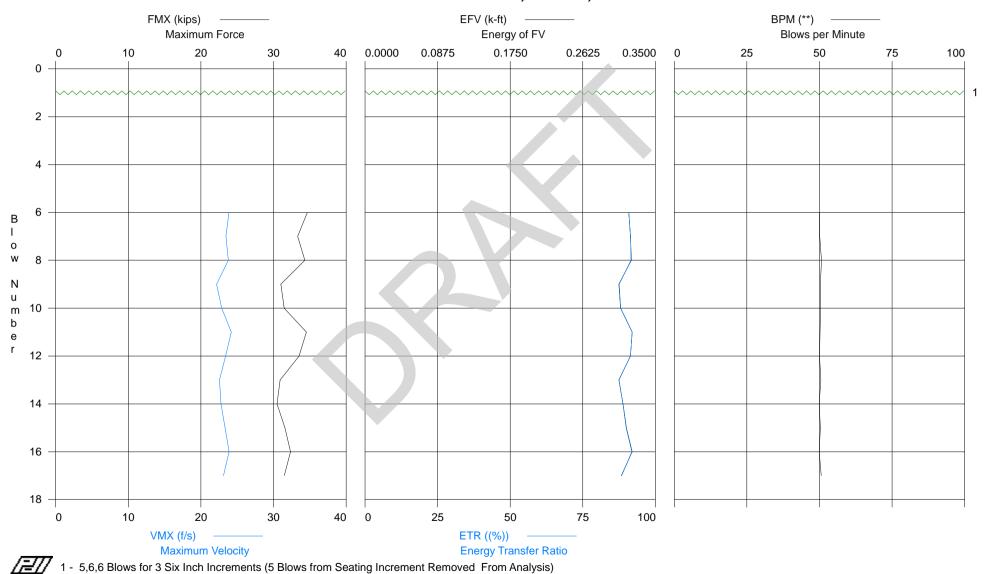
LE 28.90 ft

AR <u>Sensors</u> 1.16 in^2 30000 ksi F3: [171AWJ-1] 215.18 (1) ΕM SP 0.492 k/ft3 F4: [171AWJ-2] 214.69 (1) WS 16807.9 f/s A3: [K3540] 382 mv/5000g's (1) EA/C A4: [K2615] 285 mv/5000g's (1) 2.1 ksec/ft 2L/C 3.44 ms CLIP: OK []

Test date: 2-Dec-2013

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Southern Earth Science - SPT Hammer Calibration - SS2 @ 30 FT Diedrich D50 Automatic, SN#268, AWJ



PDIPLOT Ver. 2012.2 - Printed: 3-Dec-2013

| Southern Earth Science - SPT Hammer Calibration - SS2 @ 30 FT Diedr OP: M.J. | | | | | | | Diedrich | | matic, SN#2 est date: 2-D | |
|--|-------------|------------|------|------|------|------|----------|--------|------------------------------|-----------|
| AR: | 1.16 in^ | 2 | | | | | | | SP: 0. | 492 k/ft3 |
| LE: | 36.90 ft | | | | | | | | EM: 30, | 000 ksi |
| WS: 1 | 6,807.9 f/s | | | | | | | | JC: | 0.00 |
| | Maximum | | | | | | | BPM: B | lows per Mi | nute |
| | Maximum | | | | | | | | nergy of FV | |
| VT1: | | | | | | | | | nergy of FV | |
| | , | Displaceme | ent | | | | | | nergy Trans | |
| DFN: | Final Disp | | | | | | | | 3, | |
| BL# | depth | FMX | VMX | VT1 | DMX | DFN | BPM | E2E | EFV | ETR |
| | ft | kips | f/s | f/s | in | in | ** | k-ft | k-ft | (%) |
| 6 | 0.00 | 35 | 23.9 | 23.9 | 1.37 | 1.37 | 50.0 | 0.299 | 0.318 | 90.82 |
| 7 | 0.00 | 33 | 23.5 | 23.5 | 1.40 | 1.40 | 50.1 | 0.300 | 0.320 | 91.44 |
| 8 | 0.00 | 34 | 23.8 | 23.8 | 1.40 | 1.40 | 50.7 | 0.302 | 0.321 | 91.58 |
| 9 | 0.00 | 31 | 22.2 | 22.2 | 1.23 | 1.23 | 50.3 | 0.293 | 0.306 | 87.52 |
| 10 | 0.00 | 31 | 22.9 | 22.9 | 1.19 | 1.14 | 50.4 | 0.294 | 0.308 | 88.04 |
| 11 | 0.00 | 35 | 24.2 | 24.2 | 1.25 | 1.25 | 50.2 | 0.306 | 0.322 | 92.04 |
| 12 | 0.00 | 34 | 23.4 | 23.4 | 1.29 | 1.29 | 50.0 | 0.302 | 0.320 | 91.40 |
| 13 | 0.00 | 31 | 22.6 | 22.6 | 1.04 | 0.85 | 50.5 | 0.298 | 0.306 | 87.47 |
| 14 | 0.00 | 30 | 22.8 | 22.8 | 1.08 | 0.94 | 49.9 | 0.301 | 0.311 | 88.84 |
| 15 | 0.00 | 32 | 23.3 | 23.3 | 1.12 | 0.94 | 50.3 | 0.303 | 0.315 | 89.94 |
| 16 | 0.00 | 32 | 23.9 | 23.9 | 1.26 | 1.22 | 49.9 | 0.306 | 0.322 | 91.88 |
| 17 | 0.00 | 31 | 23.1 | 23.1 | 1.21 | 0.98 | 50.6 | 0.300 | 0.309 | 88.40 |
| | Average | 32 | 23.3 | 23.3 | 1.24 | 1.17 | 50.2 | 0.300 | 0.315 | 89.95 |

BL# depth (ft) Comments

1 0.00 5,6,6 Blows for 3 Six Inch Increments (5 Blows from Seating Increment Removed From Analys

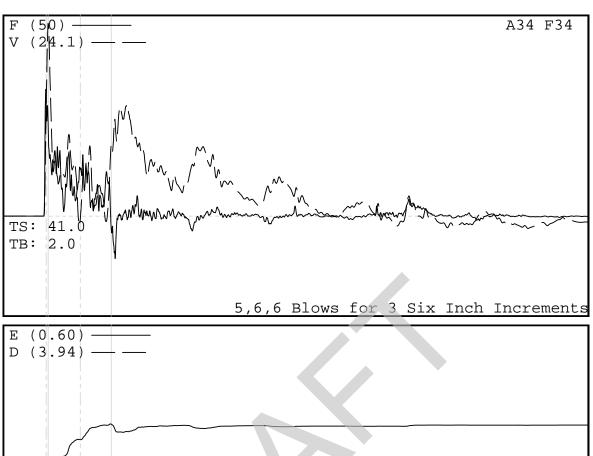
Total number of blows analyzed: 12

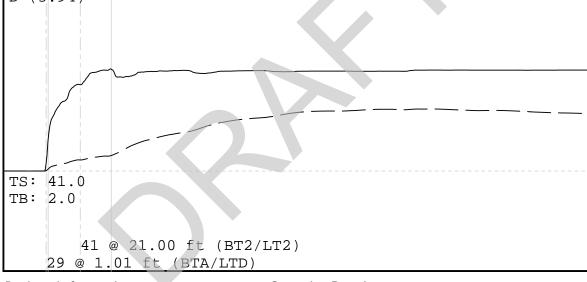
Time Summary

Drive 19 seconds 10:48:40 AM - 10:48:59 AM (12/2/2013) BN 1 - 17

Southern Earth Science - SPT Hammer Calibration

SS2 @ 30 FT





Project Information Quantity Results PROJECT: Southern Earth Science - SPT HammiFMXalib31:ikips

PILE NAME: SS2 @ 30 FT VMX 23.1 f/s DESCR: Diedrich D50 Automatic, SN#268, AWJVT1 23.1 f/s OPERATOR: M.J. DMX 1.21 in FILE: SS2 30 FT.W01 DFN 0.98 in 12/2/2013 10:48:58 AM BPM 50.6 bpm Blow Number 17 E2E 0.30 k-ft EFV 0.31 k-ft ETR 88.4 (%) Pile Properties

36.90 ft AR 1.16 in^2 30000 ksi ΕM SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.1 ksec/ft 2L/C 4.39 ms []

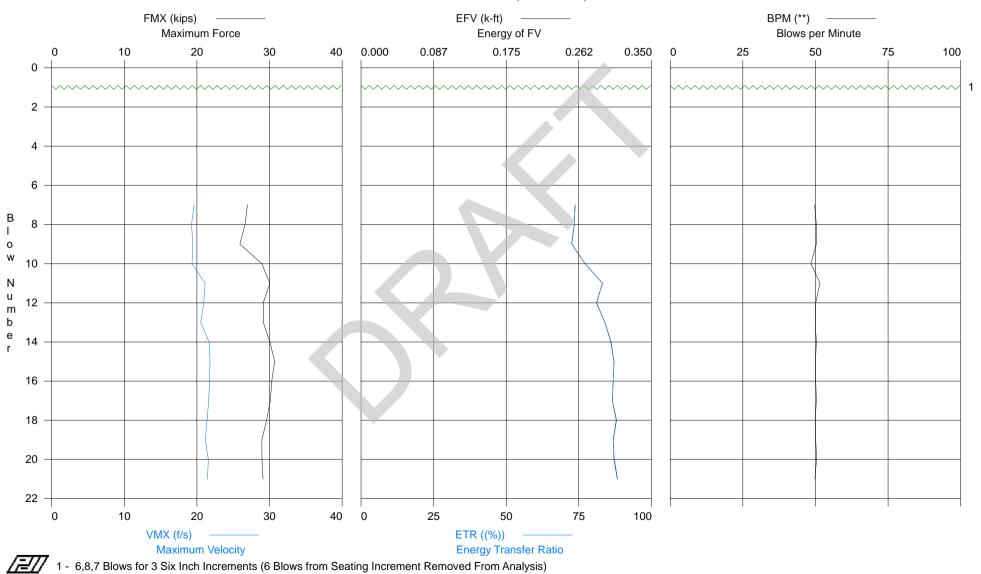
<u>Sensors</u>

F3: [171AWJ-1] 215.18 (1) F4: [171AWJ-2] 214.69 (1) A3: [K3540] 382 mv/5000g's (1) A4: [K2615] 285 mv/5000g's (1) CLIP: OK

Test date: 2-Dec-2013

PDIPLOT Ver. 2012.2 - Printed: 3-Dec-2013

Southern Earth Science - SPT Hammer Calibration - SS3 @ 35 FT Diedrich D50 Automatic, SN#268, AWJ



PDIPLOT Ver. 2012.2 - Printed: 3-Dec-2013

| Southern Earth Science - SPT Hammer Calibration - SS3 @ 35 FT OP: M.J. | | | | | | | | | matic, SN#2 est date: 2-D | |
|--|-------------|-----------|------|-------|----------|------------|-----------|--------|------------------------------|-----------|
| AR: | 1.16 in^ | 2 | | | | | | | SP: 0. | 492 k/ft3 |
| LE: | 41.90 ft | | | | | | | | EM: 30, | ,000 ksi |
| WS: 1 | 6,807.9 f/s | | | | | | | | JC: | 0.00 |
| FMX: | Maximum | Force | | | | | | BPM: B | lows per Mi | nute |
| VMX: | Maximum | Velocity | | | | | | E2E: E | nergy of FV | at 2L/c |
| VT1: | Velocity at | t Time 1 | | | | | | EFV: E | nergy of FV | ' |
| DMX: | Maximum | Displacem | ent | | | | | | nergy Trans | |
| DFN: | Final Disp | | | | | | | | | |
| BL# | depth | FMX | VMX | VT1 | DMX | DFN | BPM | E2E | EFV | ETR |
| | ft | kips | f/s | f/s | in | in | ** | k-ft | k-ft | (%) |
| 7 | 0.00 | 27 | 19.6 | 19.6 | 0.80 | -0.02 | 49.7 | 0.255 | 0.258 | 73.78 |
| 8 | 0.00 | 27 | 19.3 | 19.3 | 0.86 | 0.24 | 50.3 | 0.254 | 0.257 | 73.46 |
| 9 | 0.00 | 26 | 19.4 | 19.4 | 0.83 | -0.08 | 50.3 | 0.252 | | 72.65 |
| 10 | 0.00 | 29 | 19.3 | 19.3 | 0.97 | 0.36 | 48.4 | 0.265 | 0.270 | 77.15 |
| 11 | 0.00 | 30 | 21.1 | 21.1 | 1.03 | 0.38 | 51.6 | 0.286 | 0.291 | 83.17 |
| 12 | 0.00 | 29 | 20.9 | 20.9 | 0.95 | -0.06 | 50.1 | 0.280 | 0.284 | 81.03 |
| 13 | 0.00 | 29 | 20.5 | 20.5 | 0.92 | 0.23 | 49.9 | 0.290 | 0.294 | 84.01 |
| 14 | 0.00 | 30 | 21.7 | 21.7 | 0.77 | 0.10 | 50.3 | 0.296 | 0.301 | 86.11 |
| 15 | 0.00 | 31 | 21.8 | 21.8 | 0.70 | 0.02 | 50.0 | 0.300 | 0.305 | 87.16 |
| 16 | 0.00 | 30 | 21.7 | 21.7 | 0.72 | -0.07 | 50.1 | 0.298 | 0.304 | 86.81 |
| 17 | 0.00 | 30 | 21.6 | 21.6 | 0.79 | 0.20 | 50.3 | 0.297 | 0.303 | 86.60 |
| 18 | 0.00 | 30 | 21.4 | 21.4 | 0.85 | 0.51 | 49.9 | 0.302 | 0.308 | 87.86 |
| 19 | 0.00 | 29 | 21.1 | 21.1 | 0.81 | 0.29 | 50.1 | 0.300 | 0.304 | 86.79 |
| 20 | 0.00 | 29 | 21.6 | 21.6 | 0.80 | 0.24 | 50.4 | 0.300 | 0.305 | 87.25 |
| 21 | 0.00 | 29 | 21.5 | 21.5 | 0.81 | 0.26 | 49.8 | 0.305 | 0.309 | 88.39 |
| | Average | 29 | 20.8 | 20.8 | 0.84 | 0.17 | 50.1 | 0.285 | 0.290 | 82.81 |
| | | | | Total | number o | f blows ar | alyzed: 1 | 5 | | |

BL# depth (ft) Comments

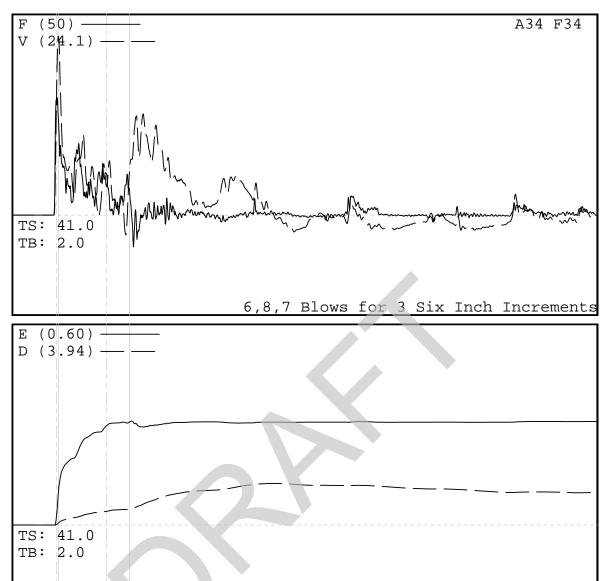
1 0.00 6,8,7 Blows for 3 Six Inch Increments (6 Blows from Seating Increment Removed From Analysi

Time Summary

Drive 24 seconds 11:09:58 AM - 11:10:22 AM (12/2/2013) BN 1 - 21

Southern Earth Science - SPT Hammer Calibration

SS3 @ 35 FT



| <u>Project Information</u> | <u>Quantity Results</u> |
|--|--------------------------------|
| PROJECT: Southern Earth Science - SPT Hamn | nFMXalib29:ikips |
| PILE NAME: SS3 @ 35 FT | VMX 21.5 f/s |
| DESCR: Diedrich D50 Automatic, SN#268, AW | /JVT1 21.5 f/s |
| OPERATOR: M.J. | DMX 0.81 in |
| FILE: SS3 35 FT.W01 | DFN 0.26 in |
| 12/2/2013 11:10:21 AM | BPM 49.8 bpm |
| Blow Number 21 | E2E 0.30 k-ft |
| | EFV 0.31 k-ft |
| <u>Pile Properties</u> | ETR 88.4 (%) |
| LE 41.90 ft | |
| AR 1.16 in^2 | <u>Sensors</u> |
| EM 30000 ksi | F3: [171AWJ-1] 215.18 (1) |
| SP 0.492 k/ft3 | F4: [171AWJ-2] 214.69 (1) |
| WS 16807.9 f/s | A3: [K3540] 382 mv/5000g's (1) |
| EA/C 2.1 ksec/ft | A4: [K2615] 285 mv/5000g's (1) |
| 2L/C 4.98 ms | CLIP: OK |
| JC [] | |

52 @ 30.46 ft (BT2/LT2)

38 @ 1.01 ft (BTA/LTD)

6100 Hillcroft, Houston, Texas 77081 Tel: 713-369-5400 www.fugroconsultants.com



SPT Calibration Report – Fugro Drill Rig SN#361982

Project No: 04.55124092

To: Jennifer Aguettant

Project Manager

From: Michael A. Norfleet, P.E.

Date: September 25, 2013

Subject: SPT Hammer Energy Calibrations

Fugro Consultants, Inc. (Fugro) is pleased to present the results of the Standard Penetration Test (SPT) energy calibration measurements conducted on September 20, 2013 at the Fugro Facilities Yard, in Houston, Texas.

Purpose and Scope. The purpose of SPT energy calibration described herein is to determine the average energy transferred from the exploration rig's hammer to the drilling rods during SPT sampling. The energy testing methods are described in the ASTM D4633 Standard Test Method for Energy Measurement of Dynamic Penetrometers. The measured energy may then be used to correct the measured SPT N-values to a standardized energy level, typically 60% of the theoretical energy (N_{60}) .

Summary of Scope:

- mobilize PDA equipment and personnel to the drill rig location,
- provide energy calibrations by measuring the force (from strain) and velocity (from acceleration) using an instrumented rod section and a PDA.
- present the test results and findings.

Test Summary

Instrumentation and Test Sequence. SPT energy testing was performed in general accord with ASTM D4633 using the Pile Driving Analyzer (PDA) model PAX (SN 3846L) in conjunction with an instrumented 2-foot section of NWJ drilling rod (SN 333NWJ), both manufactured by Pile Dynamics, Inc. of Cleveland, Ohio. The instrumented rod consists of two strain sensors in full-bridge configuration with each strain bridge mounted to cancel any bending in the rod section. Attachment 1 includes a calibration certificate for the rod section. Two accelerometers are also bolted directly to the rod section during data collection. To collect data, the instrumented rod section was threaded tightly onto the top of the drill-rod string, just underneath the SPT hammer. For selected sampling intervals, the PDA digitized and stored strain and acceleration data at a sampling rate of 100 kHz for each impact of the SPT hammer. During the hammer impact, the

Calibration Report - Fugro Drill Rig #361982



PDA multiplied the strain wave by the rod area and modulus to obtain the force wave, and integrated the acceleration to obtain the velocity wave. By integrating the product of force and velocity over the time of the impact, the PDA can then determine the net energy delivered to the sample rods during each blow. The PDA operator reviewed the results, performed data quality checks, and obtained an adequate number and range of sample SPT blows to properly characterize the hammer energy performance for Fugro Drill Rig #361982 tested.

The automatic SPT hammer was operated by the lead driller on Rig #361982. The drill rig used NWJ drill rods. Fugro tested the attached automatic hammer for this report, which had no serial number or identifying marks. The automatic hammer was completely encased for safety reasons and appeared to be in good operating condition. During normal drilling operations on Rig #361982 four data sets were collected as listed below in Table 1 (exceeding the minimum of three required by ASTM D4633). Each table includes the date, location, sample starting depths, the blow count for each 6-inch depth interval, and the uncorrected N-value (sum of last two blow counts).

Table 1: Summary of SPT Data Sets – Automatic Hammer on Rig #361982

| Test Date | Data Set No. | Boring Location | Sample Depth | 150mm Blow Counts and N-value |
|--------------|-----------------|--------------------|-----------------|----------------------------------|
| 09-20-13 | SPT-1 | Fugro Yard | 10 ft | 3 / 2 / 2 N=4 |
| 09-20-13 | SPT-2 | Fugro Yard | 12 ft | 2 / 3 / 4 N=7 |
| 09-20-13 | SPT-3 | Fugro Yard | 14 ft | 7 / 7 / 9 N=16 |
| 09-20-13 | SPT-4 | Fugro Yard | 16 ft | 17 / 21 / 24 N=45 |

Evaluation of SPT Energy. Test results were evaluated utilizing the F-V energy method described in ASTM D4633. The PDA computes EMX, the energy transferred to the rods as measured at the gage location using force, F(t), and velocity, v(t), by the following equation:

$$EMX = EFV = \int_{0}^{b} F(t) \cdot v(t) dt$$

The time "a" corresponds to the start of the record just before impact of the hammer and "b" is the time the energy transferred reaches a maximum value.

Calibration Report - Fugro Drill Rig #361982



Discussion of SPT Calibration Results

In Attachment 2 we present field notes, wave traces for representative hammer blows, and plots and tables prepared from the PDA data for each data set. Each PDA plot contains three main graphs. The left-hand graph shows CSX (maximum average compressive stress) and CSI (maximum individual gage stress) plotted versus blow number. Together these plots show the difference between the two force measurements. The center plot shows EMX (maximum energy) and ETR (EMX divided by theoretical hammer energy). These plots indicate the hammer efficiency and consistency during testing. The right-hand graph shows FMX (maximum force) and BPM (blows per minute) to give a relative hammer "operational performance" during testing. The tabulated output for each data set also includes statistical evaluations: average, maximum, minimum, and standard deviation. To arrive at overall performance of the hammer tested, we used the average statistical evaluations from the data sets, shown in Table 2.

The uncorrected N-values can be corrected using the following equations:

$$N_{60} = N_{measured} x Correction Factor$$

$$N_{60} = N_{\text{measured}} \times (ETR/60\%)$$

The average value of all the ETR values for each data set was used in the above equation to calculate an average correction factor. These correction factors may be applied to N-values from sampling intervals in these and other borings not tested with the PDA, provided the hammers are not modified and are maintained in their current condition.

Table 2: Summary of SPT Results – Automatic Hammer on Rig #361982

| Data Set | ВРМ | FMX (kips) | EMX (k-ft) | ETR (%) | N _{measured} | N ₆₀ |
|--------------------------------|-----|---------------|---------------|------------|--------------------------|-----------------|
| SPT-1 | 32 | 39 | 0.264 | 76 | 4 | 6 |
| SPT-2 | 47 | 41 | 0.337 | 96 | 7 | 10 |
| SPT-3 | 44 | 40 | 0.290 | 83 | 16 | 23 |
| SPT-4 | 50 | 40 | 0.307 | 88 | 45 | 64 |
| Average Overall Performance | 43 | 40 | 0.300 | 86 | Correction Factor = 1.43 | |

Calibration Report - Fugro Drill Rig #361982



Conclusions

Fugro obtained SPT energy measurements for one automatic hammer attached to Fugro Drill Rig #361982 during sampling events on 9/20/2013 in the Fugro Facilities Yard. The hammer appeared to be operating normally. Tables 1 to 2 above summarize the data collected and the average calculated transferred energies in accordance with ASTM D4633. On average, the ETR, Energy Transfer Ratio, was 86% for the automatic hammer attached to Fugro Drill Rig #361982.

We appreciate the opportunity to be of service. Please call us if you have any questions or comments concerning the field notes, SPT plots and tables, or when we may be of further assistance.

Sincerely,

FUGRO CONSULTANTS, INC.

Michael Norfleet, P.E. Sr. Project Professional

Attachments:

Attachment 1: Test Photos and Sensor Calibrations

Attachment 2: Fugro Drill Rig #361982 SPT Test Records and Field Notes

FUGRO CONSULTANTS, INC. Calibration Report – Fugro Drill Rig #361982



ATTACHMENT #1

Test Photos and Sensor Calibrations





Rig #361982 Plaque



Striking Surface Attachment to Instrumented Rod

FUGRO CONSULTANTS, INC. Calibration Report – Fugro Drill Rig #361982



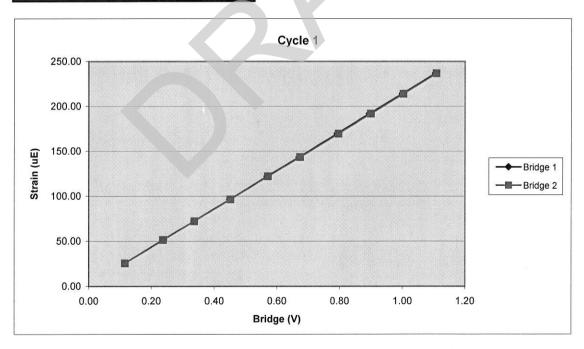


Mounted Automatic Hammer on Rig #361982

| 333NWJ | | Cycle 1 | | |
|--------|------------|-------------|--------------|--------------|
| Sample | Force (lb) | Strain (µE) | Bridge 1 (V) | Bridge 2 (V) |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 1038.93 | 25.63 | 0.12 | 0.12 |
| 3 | 2112.50 | 51.34 | 0.24 | 0.24 |
| 4 | 2998.51 | 72.10 | 0.34 | 0.34 |
| 5 | 4030.95 | 96.42 | 0.45 | 0.45 |
| 6 | 5109.63 | 121.88 | 0.57 | 0.57 |
| 7 | 6031.46 | 143.53 | 0.67 | 0.67 |
| 8 | 7140.85 | 169.65 | 0.79 | 0.80 |
| 9 | 8079.21 | 191.78 | 0.90 | 0.90 |
| 10 | 9034.10 | 214.09 | 1.00 | 1.00 |
| 11 | 9994.90 | 236.67 | 1.11 | 1.11 |

| Bridge 1 | | Bridge 2 | |
|---------------------------|----------|---------------------------|----------|
| Force Calibration (lb/V) | 9062.28 | Force Calibration (lb/V) | 9020.00 |
| Offset | -38.24 | Offset | -28.48 |
| Correlation | 0.999990 | Correlation | 0.999989 |
| Strain Calibration (µE/V) | 213.39 | Strain Calibration (µE/V) | 212.39 |
| Offset | 0.56 | Offset | 0.79 |
| Correlation | 0.999996 | Correlation | 0.999994 |

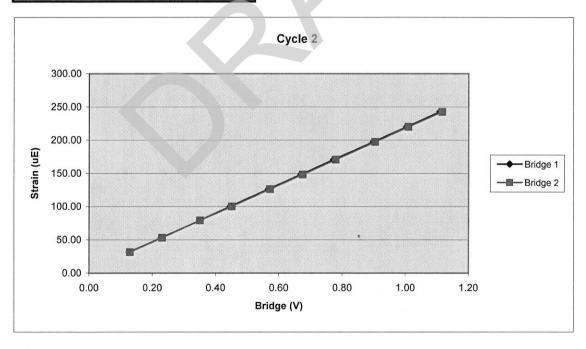
| Force Strain Calibration | |
|--------------------------|----------|
| EA (Kips) | 42468.92 |
| Offset | -61.97 |
| Correlation | 0.999998 |



| 333NWJ | | Cycle 2 | | |
|--------|------------|-------------|--------------|--------------|
| Sample | Force (lb) | Strain (µE) | Bridge 1 (V) | Bridge 2 (V) |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 1138.32 | 31.42 | 0.13 | 0.13 |
| 3 | 2045.78 | 53.13 | 0.23 | 0.23 |
| 4 | 3129.98 | 79.01 | 0.35 | 0.35 |
| 5 | 4010.08 | 99.98 | 0.45 | 0.45 |
| 6 | 5118.68 | 126.12 | 0.57 | 0.57 |
| 7 | 6067.28 | 148.26 | 0.67 | 0.67 |
| 8 | 7005.84 | 170.48 | 0.77 | 0.78 |
| 9 | 8154.78 | 197.38 | 0.90 | 0.90 |
| 10 | 9110.07 | 219.90 | 1.00 | 1.01 |
| 11 | 10089.37 | 242.56 | 1.11 | 1.12 |

| Bridge 1 | | Bridge 2 | |
|---------------------------|----------|---------------------------|----------|
| Force Calibration (lb/V) | 9123.54 | Force Calibration (lb/V) | 9074.39 |
| Offset | -49.69 | Offset | -53.66 |
| Correlation | 0.999993 | Correlation | 0.999988 |
| Strain Calibration (µE/V) | 215.17 | Strain Calibration (µE/V) | 214.02 |
| Offset | 3.89 | Offset | 3.79 |
| Correlation | 0.999998 | Correlation | 0.999998 |

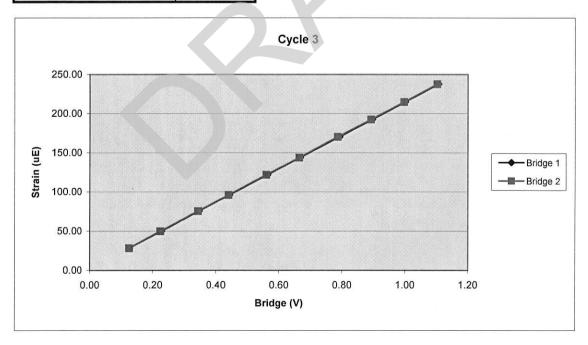
| Force Strain Calibration | |
|--------------------------|----------|
| EA (Kips) | 42400.74 |
| Offset | -214.40 |
| Correlation | 0.999992 |



| 333NWJ | | Cycle 3 | | |
|--------|------------|-------------|--------------|--------------|
| Sample | Force (lb) | Strain (µE) | Bridge 1 (V) | Bridge 2 (V) |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 1125.52 | 28.24 | 0.13 | 0.12 |
| 3 | 2016.06 | 49.68 | 0.23 | 0.22 |
| 4 | 3101.05 | 75.29 | 0.35 | 0.34 |
| 5 | 3977.02 | 95.97 | 0.44 | 0.44 |
| 6 | 5073.81 | 121.83 | 0.56 | 0.56 |
| 7 | 6005.68 | 143.75 | 0.67 | 0.66 |
| 8 | 7133.76 | 170.21 | 0.79 | 0.79 |
| 9 | 8082.95 | 192.52 | 0.90 | 0.89 |
| 10 | 9043.75 | 214.97 | 1.00 | 1.00 |
| 11 | 10017.53 | 237.71 | 1.11 | 1.10 |

| Bridge 1 | | Bridge 2 | |
|---------------------------|----------|---------------------------|----------|
| Force Calibration (lb/V) | 9067.17 | Force Calibration (lb/V) | 9087.50 |
| Offset | -32.75 | Offset | -17.10 |
| Correlation | 0.999991 | Correlation | 0.999996 |
| Strain Calibration (µE/V) | 213.44 | Strain Calibration (µE/V) | 213.91 |
| Offset | 1.42 | Offset | 1.79 |
| Correlation | 0.999998 | Correlation | 0.999998 |

| Force Strain Calibration | |
|--------------------------|----------|
| EA (Kips) | 42481.93 |
| Offset | -93.13 |
| Correlation | 0.999995 |



Bridge Excitation (V) Shunt Resitor (ohm)

60.4k

| Calibration Factors | 333NWJ | | |
|---------------------|----------|-----------------|--------|
| Bridge 1 (μΕ/V) | 214.00 | Bridge 2 (µE/V) | 213.44 |
| EA Factor (Kips) | 42450.53 | Area (in^2) | 1.42 |

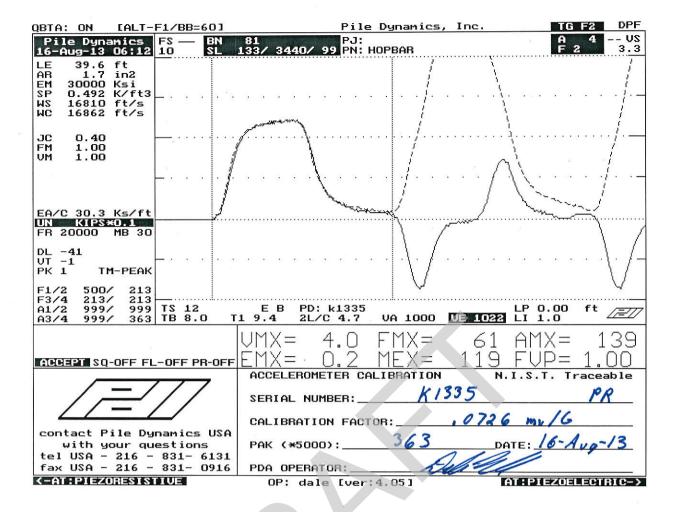
Calibrated by:

Calibrated Date:

3/26/2013

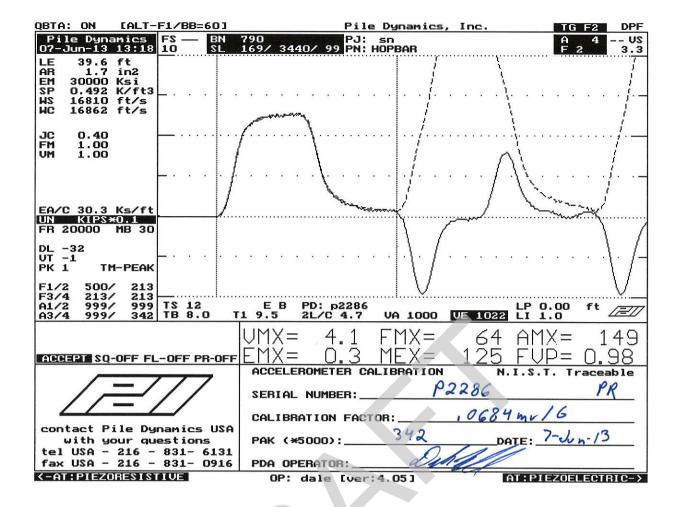
Pile Dynamics Inc 30725 Aurora Rd Solon, OH 44139

Traceable to N.I.S.T.



Smart Sensor

Smart Chip Programmed By DB on 16-Avg-/3 CRC Value A6BF



FUGRO CONSULTANTS, INC. Calibration Report – Fugro Drill Rig #361982



ATTACHMENT #2

Fugro Drill Rig #361982 SPT Records and Field Notes



Fugro Consultants, Inc.

6100 Hillcroft, 77081 P.O. Box 740010 Houston, TX 77274 Ph: (713) 369-5400 F (713) 369-5518

| Project # | 04.55124092 |
|-----------------|---------------------|
| Project Name | |
| SPT Tester | Michael Norfleet |
| Rig(s) | CME 850 - SN#361982 |
| Rig Operator(s) | Jose |
| Test Date(s) | 9/20/13 |

SPT ENERGY CALIBRATION – HAMMER: Rig #361982

| CME 850 Track mounted Drill Rig, Serial Number #361982 | |
|--|--|
| Automatic hammer attached, no identifying marks | |
| | |
| | |
| | |

Notes on Operational Performance

| | or on operational continuation |
|----|--|
| Ha | mmer appears to be in good operational conditions |
| | |
| "[| " - Effective Length of Pod Sections input into SPT Analyzor |

Instrumentation

| Name: 333NWJ Area: 1.42 in ² | |
|--|--|
| Strains: F3: 333NWJ-1, Gage Factor = 214.00 με/V | Accelerometers: A3: K1335, Gage Factor = 363 (mV/G x 5000) |
| F4: 320NWJ-2, Gage Factor = 213.44 με/V | Accelerometers: A4: P2286, Gage Factor = 342 (mV/G x 5000) |

| Data Set 1 | Location: Fugro Yard | Rig | 361962 | Time: 9/20/13 10:05 |
|----------------------|----------------------------|-----|----------------|------------------------------------|
| Starting depth of s | ample | | 10ft | |
| Gage location from | n tip of sampler "LE" | | "LE" = 35.5in | + 120in + 10in = 165.5in = 13.79ft |
| List of rod sections | from sampler to instrument | | Sampler / [5ft | t x 2] / Instrument / Hammer |
| Length from impac | et surface to gages | | 18 inches | |
| Blows observed (u | ncorrected) | | 3/2/2 per 6 | inches N=4 |

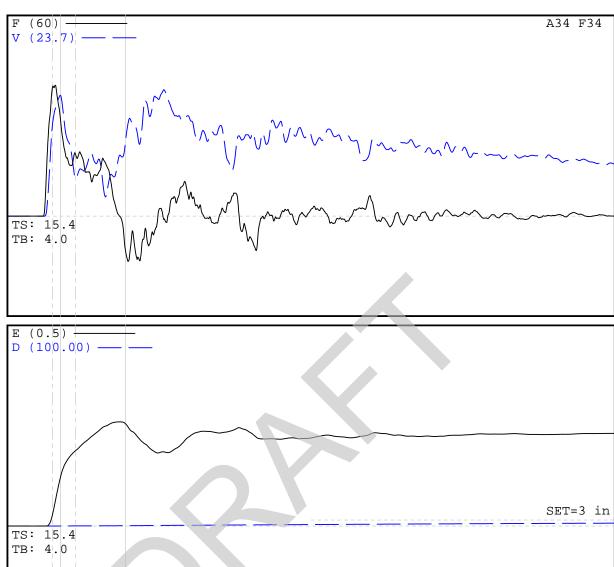
| Data Set 2 | Location: Fugro Yard | Rig: | 361962 | Time: 9/20/13 15:57 |
|---------------------|-------------------------------|------|----------------------|---------------------------------------|
| Starting depth of | sample | | 12ft | |
| Gage location fro | m tip of sampler "LE" | | "LE" = 35.5in + 12 | 0in + 60in + 10in = 225.5in = 18.79ft |
| List of rod section | is from sampler to instrument | | Sampler / [10ft][5ft | t] / Instrument / Hammer |
| Length from impa | act surface to gages | | 18 inches | |
| Blows observed (| uncorrected) | | 2/3/4 per 6 inch | es N=7 |

| Data Set 3 | Location: Fugro Yard | Rig: | 361962 | Time: 9/20/13 10:19 |
|---------------------|-------------------------------|------|---------------------|--|
| Starting depth of | sample | | 14ft | |
| Gage location fro | m tip of sampler "LE" | | "LE" = 35.5in + 1 | 20in + 60in + 10in = 225.5in = 18.79ft |
| List of rod section | ns from sampler to instrument | | Sampler / [10ft][| 5ft] / Instrument / Hammer |
| Length from impa | act surface to gages | | 18 inches | |
| Blows observed (| uncorrected) | | 7 / 7 / 9 per 6 inc | ches N=16 |

| Data Set 4 | Location : Fugro Yard | Rig: | 361962 | Time: 9/20/13 10:40 |
|---------------------|-------------------------------|------|--------------------|--|
| Starting depth of | sample | | 16ft | |
| Gage location fro | om tip of sampler "LE" | | "LE" = 35.5in + 1 | 120in + 120in + 10in = 285.5in = 23.79ft |
| List of rod section | ns from sampler to instrument | | Sampler / [10ft][| 10ft] / Instrument / Hammer |
| Length from impa | act surface to gages | | 18 inches | |
| Blows observed | (uncorrected) | | 17 / 21 / 24 per 6 | 6 inches N=45 |

04.55124092

SPT-1 RIG 361982 10FT FUGRO YARD



Project Information

PROJECT: 04.55124092

PILE NAME: SPT-1 RIG 361982 10FT FUGRO YACSI 27.9 ksi

46 @ 6.55 ft 35 @ 1.68 ft

DESCR: SAMPLE 10FT OPERATOR: MAN

FILE: SPT-1 RIG 361982 10FT FUGRO YARD

9/20/2013 11:14:50 AM

Blow Number 4

Pile Properties

LE 13.79 ft
AR 1.42 in^2
EM 30000 ksi
SP 0.492 k/ft3
WS 16807.9 f/s
EA/C 2.5 ksec/ft
2L/C 1.64 ms

JC [] LP 10.75 ft

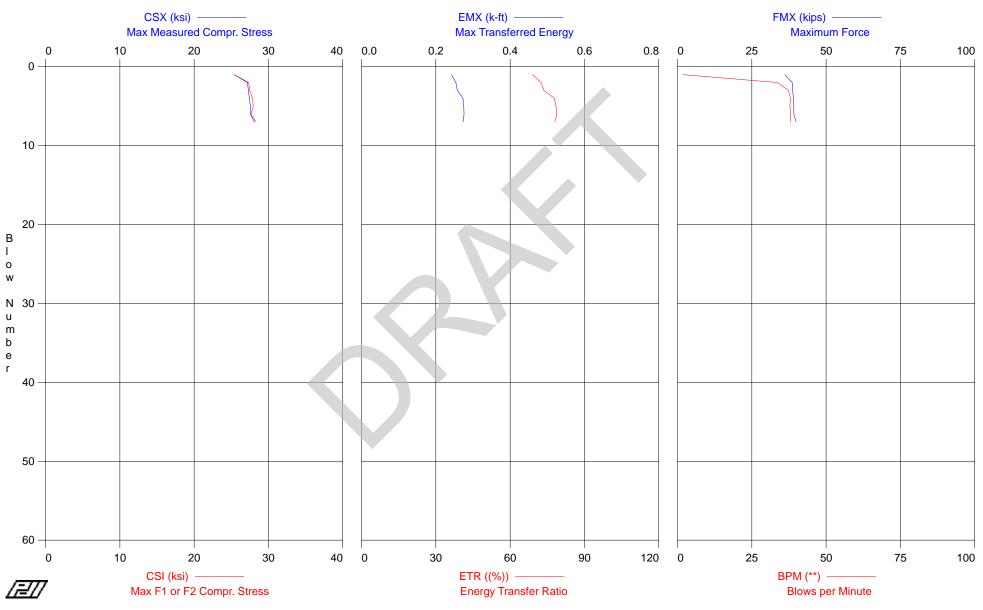
Quantity Results

CSX 27.4 ksi
ACSI 27.9 ksi
EMX 0.3 k-ft
ETR 77.9 (%)
FMX 39 kips
BPM 38.0 bpm
QNV 0.00 []
QNV 0.00 []
QNV 0.00 []

<u>Sensors</u>

F3: [SPT-333NWJ-1] 214 (1) F4: [SPT-333NWJ-2] 213.44 (1) A3: [K1335] 363 mv/5000g's (1) A4: [2286] 342 mv/5000g's (1) CLIP: OK

04.55124092 - SPT-1 RIG 361982 10FT FUGRO YARD



Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 25-Sep-2013

SAMPLE 10FT 04.55124092 - SPT-1 RIG 361982 10FT FUGRO YARD

| OP: MAN | Test date: 20-Sep-2013 |
|------------------|------------------------|
| AR: 1.42 in^2 | SP: 0.492 k/ft3 |
| LE: 13.79 ft | EM: 30,000 ksi |
| WS: 16,807.9 f/s | JC: 0.00 |
| 00V MM | ETD. E T (c. D. C. |

| | leasured Compr. | | | | | ETR: Energy Tra | |
|-------------|-------------------|-------|-----|-------|-----|-----------------|--------|
| CSI: Max F | 1 or F2 Compr. S | tress | | | | FMX: Maximum | Force |
| EMX: Max Ti | ransferred Energy | y | | | | BPM: Blows per | Minute |
| BL# | BLC | CSX | CSI | EMX | ETR | FMX | BPM |
| | bl/ft | ksi | ksi | k-ft | (%) | kips | ** |
| 1 | 6 | 25 | 25 | 0.242 | 69 | 36 | 2 |
| 2 | 6 | 27 | 27 | 0.254 | 73 | 39 | 34 |
| 3 | 6 | 27 | 27 | 0.258 | 74 | 39 | 37 |
| 4 | 4 | 27 | 28 | 0.273 | 78 | 39 | 38 |
| 5 | 4 | 28 | 28 | 0.275 | 79 | 39 | 38 |
| 6 | 4 | 28 | 28 | 0.276 | 79 | 39 | 38 |
| 7 | 4 | 28 | 28 | 0.273 | 78 | 40 | 38 |
| Average | | 27 | 27 | 0.264 | 76 | 39 | 32 |
| Std. Dev. | | 1 | 1 | 0.012 | 4 | 1 | 12 |
| Maximum | | 28 | 28 | 0.276 | 79 | 40 | 38 |
| @ Blow# | | 7 | 7 | 6 | 6 | 7 | 6 |
| Minimum | | 25 | 25 | 0.242 | 69 | 36 | 2 |
| @ Blow# | | 1 | 1 | 1 | 1 | 1 | 1 |
| | | | | | | | |

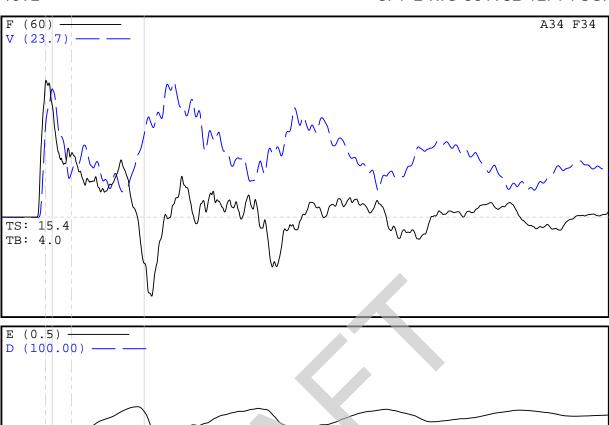
1 1 Total number of blows analyzed: 7

Time Summary

11:14:45 AM - 11:14:55 AM (9/20/2013) BN 1 - 7 Drive 10 seconds

04.55124092

SPT-2 RIG 361982 12FT FUGRO YARD



SET=2 in TS: 15.4 TB: 4.0 42 @ 6.72 ft 30 @ 1.38 ft

Project Information PROJECT: 04.55124092

PILE NAME: SPT-2 RIG 361982 12FT FUGRO YACSI 29.0 ksi

DESCR: SAMPLE 12FT OPERATOR: MAN

FILE: SPT-2 RIG 361982 12FT FUGRO YARD

9/20/2013 11:28:47 AM

Blow Number 4

Pile Properties

LE 18.79 ft AR 1.42 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.5 ksec/ft 2L/C 2.32 ms JC LP 12.83 ft

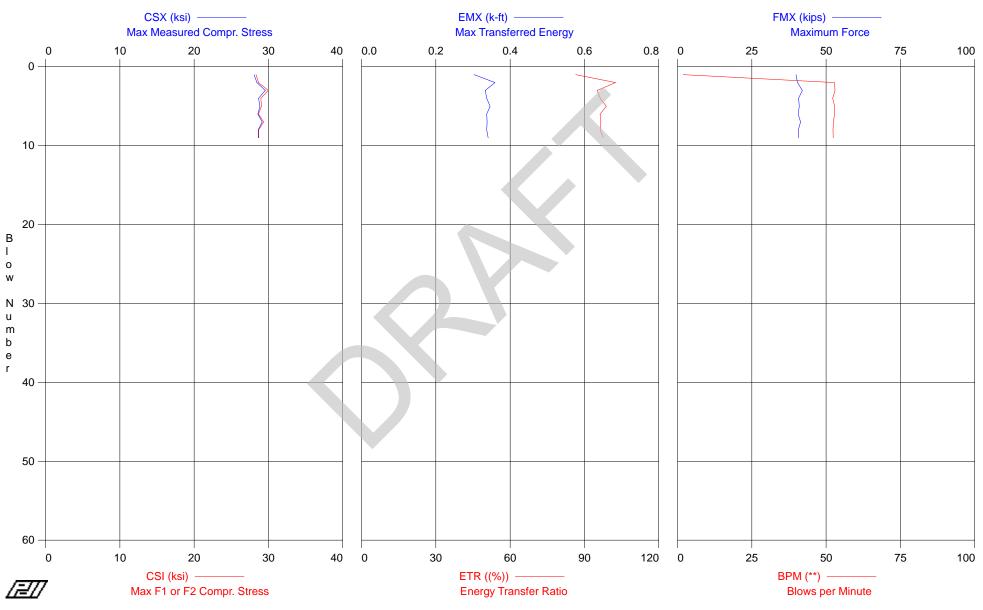
Quantity Results

CSX 28.7 ksi EMX 0.3 k-ft ETR 96.4 (%) FMX 41 kips BPM 52.2 bpm QNV 0.00 [] QNV 0.00 [] QNV 0.00 []

<u>Sensors</u>

F3: [SPT-333NWJ-1] 214 (1) F4: [SPT-333NWJ-2] 213.44 (1) A3: [K1335] 363 mv/5000g's (1) A4: [2286] 342 mv/5000g's (1) CLIP: OK

04.55124092 - SPT-2 RIG 361982 12FT FUGRO YARD



Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 25-Sep-2013

| | • |
|--|------------------------|
| 04.55124092 - SPT-2 RIG 361982 12FT FUGRO YARD | SAMPLE 12FT |
| OP: MAN | Test date: 20-Sep-2013 |

| OP: MAN | Test date: 20-Sep-2013 |
|---------------------------------|----------------------------|
| AR: 1.42 in^2 | SP: 0.492 k/ft3 |
| LE: 18.79 ft | EM: 30,000 ksi |
| WS: 16,807.9 f/s | JC: 0.00 |
| CSY: Max Massured Compr. Stress | ETD: Energy Transfer Patio |

| VV3. 10,607.8 | 7 1/5 | | | | | JC. | 0.00 |
|---------------|------------------|--------------|-------|-------|-----|-----------------|--------|
| CSX: Max M | easured Compr. | Stress | | | | ETR: Energy Tra | |
| CSI: Max F | 1 or F2 Compr. S | FMX: Maximum | Force | | | | |
| EMX: Max Ti | ansferred Energy | y | | | | BPM: Blows per | Minute |
| BL# | BLC | CSX | CSI | EMX | ETR | FMX | BPM |
| | bl/ft | ksi | ksi | k-ft | (%) | kips | ** |
| 1 | 4 | 28 | 28 | 0.303 | 86 | 40 | 2 |
| 2 | 4 | 28 | 29 | 0.359 | 103 | 40 | 53 |
| 3 | 6 | 30 | 30 | 0.333 | 95 | 42 | 53 |
| 4 | 6 | 29 | 29 | 0.337 | 96 | 41 | 52 |
| 5 | 6 | 29 | 29 | 0.346 | 99 | 41 | 53 |
| 6 | 8 | 29 | 29 | 0.337 | 96 | 41 | 53 |
| 7 | 8 | 29 | 29 | 0.338 | 97 | 41 | 53 |
| 8 | 8 | 29 | 29 | 0.337 | 96 | 41 | 52 |
| 9 | 8 | 29 | 29 | 0.341 | 98 | 41 | 52 |
| Average | | 29 | 29 | 0.337 | 96 | 41 | 47 |
| Std. Dev. | | 0 | 0 | 0.014 | 4 | 1 | 16 |
| Maximum | | 30 | 30 | 0.359 | 103 | 42 | 53 |
| @ Blow# | | 3 | 3 | 2 | 2 | 3 | 3 |
| Minimum | | 28 | 28 | 0.303 | 86 | 40 | 2 |
| @ Blow# | | 1 | 1 | 1 | 1 | 1 | 1 |
| | | | | | | | |

1 Total number of blows analyzed: 9

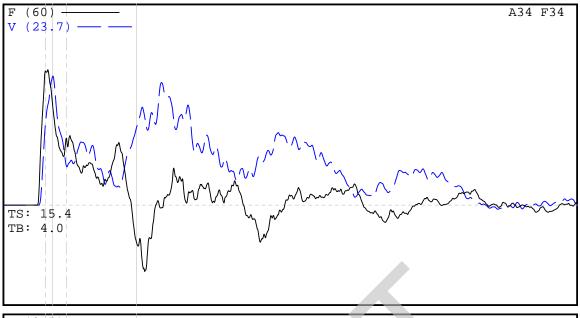
Time Summary

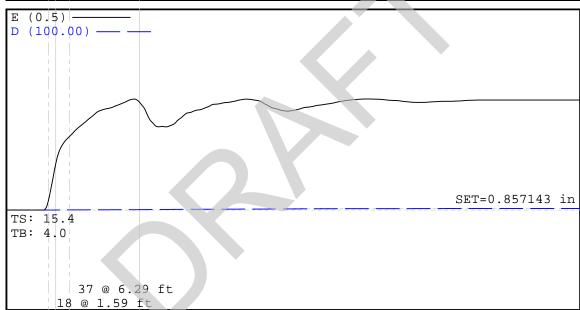
Drive 9 seconds

11:28:44 AM - 11:28:53 AM (9/20/2013) BN 1 - 9

04.55124092

SPT-3 RIG 361982 14FT FUGRO YARD





Project Information PROJECT: 04.55124092

PILE NAME: SPT-3 RIG 361982 14FT FUGRO YACSI 28.5 ksi

DESCR: SAMPLE 12FT OPERATOR: MAN

FILE: SPT-3 RIG 361982 14FT FUGRO YARD 9/20/2013 11:45:23 AM

Blow Number 9

Pile Properties

LE 18.79 ft AR 1.42 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.5 ksec/ft 2L/C 2.24 ms JC 14.64 ft LP

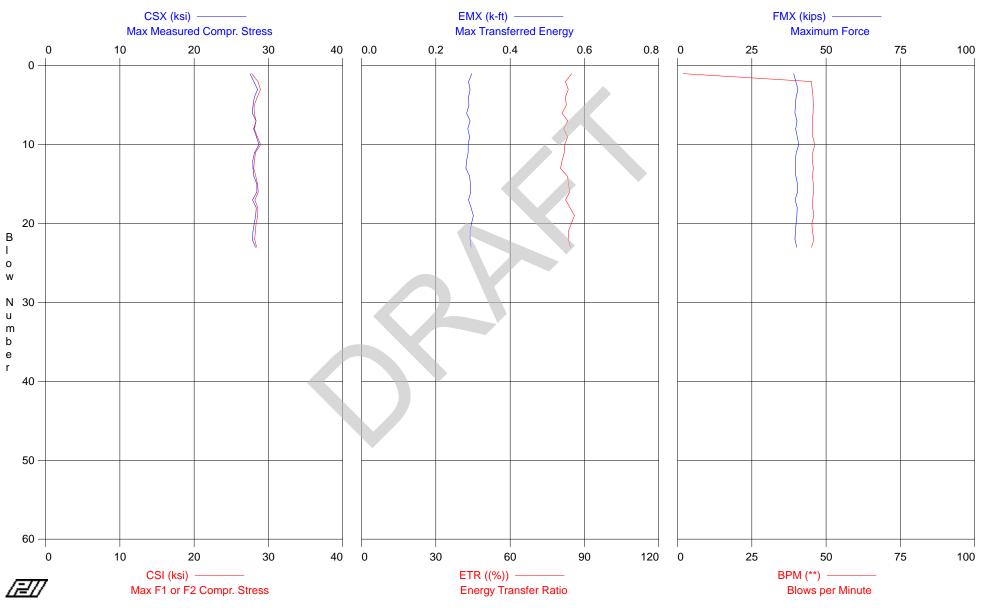
Quantity Results

CSX 28.4 ksi EMX 0.3 k-ft ETR 83.2 (%) FMX 40 kips BPM 45.5 bpm QNV 0.00 [] QNV 0.00 [] QNV 0.00 []

<u>Sensors</u>

F3: [SPT-333NWJ-1] 214 (1) F4: [SPT-333NWJ-2] 213.44 (1) A3: [K1335] 363 mv/5000g's (1) A4: [2286] 342 mv/5000g's (1) CLIP: OK

04.55124092 - SPT-3 RIG 361982 14FT FUGRO YARD



Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 25-Sep-2013

04.55124092 - SPT-3 RIG 361982 14FT FUGRO YARD SAMPLE 12FT

 OP: MAN
 Test date: 20-Sep-2013

 AR: 1.42 in^2
 SP: 0.492 k/ft3

 LE: 18.79 ft
 EM: 30,000 ksi

 WS: 16,807.9 f/s
 JC: 0.00

| CSI: | Max Measured Compr. St Max F1 or F2 Compr. Str Max Transferred Energy | | | | | ETR: Energy Tra FMX: Maximum BPM: Blows per | Force |
|--------|---|-----|-------|--------------------|-------------|---|-------|
| BL# | BLC | CSX | CSI | EMX | ETR | FMX | BPM |
| | bl/ft | ksi | ksi | k-ft | (%) | kips | ** |
| 1 | 14 | 28 | 28 | 0.297 | 85 | 39 | 2 |
| 2 | 14 | 28 | 29 | 0.288 | 82 | 40 | 45 |
| 3 | 14 | 29 | 29 | 0.292 | 83 | 41 | 45 |
| 4 | 14 | 28 | 28 | 0.288 | 82 | 40 | 46 |
| 5 | 14 | 28 | 28 | 0.289 | 83 | 40 | 46 |
| 6 | 14 | 28 | 28 | 0.283 | 81 | 40 | 46 |
| 7 | 14 | 28 | 28 | 0.292 | 83 | 40 | 45 |
| 8 | 14 | 28 | 28 | 0.286 | 82 | 40 | 45 |
| 9 | 14 | 28 | 29 | 0.291 | 83 | 40 | 46 |
| 10 | 14 | 29 | 29 | 0.287 | 82 | 41 | 46 |
| 11 | 14 | 28 | 28 | 0.287 | 82 | 40 | 46 |
| 12 | 14 | 28 | 28 | 0.283 | 81 | 40 | 45 |
| 13 | 14 | 28 | 28 | 0.281 | 80 | 40 | 46 |
| 14 | 14 | 28 | 28 | 0.291 | 83 | 40 | 45 |
| 15 | 18 | 28 | 29 | 0.293 | 84 | 40 | 46 |
| 16 | 18 | 28 | 29 | 0.294 | 84 | 40 | 46 |
| 17 | 18 | 28 | 28 | 0.288 | 82 | 40 | 46 |
| 18 | 18 | 28 | 29 | 0.295 | 84 | 40 | 46 |
| 19 | 18 | 28 | 29 | 0.301 | 86 | 40 | 46 |
| 20 | 18 | 28 | 28 | 0.296 | 85 | 40 | 45 |
| 21 | 18 | 28 | 28 | 0.292 | 84 | 40 | 45 |
| 22 | 18 | 28 | 28 | 0.292 | 83 | 40 | 46 |
| 23 | 18 | 28 | 28 | 0.295 | 84 | 40 | 45 |
| Averag | ge | 28 | 28 | 0.290 | 83 | 40 | 44 |
| Std. D | | 0 | 0 | 0.005 | 1 | 0 | 9 |
| Maxim | ium | 29 | 29 | 0.301 | 86 | 41 | 46 |
| @ Blo | w# | 10 | 10 | 19 | 19 | 10 | 10 |
| Minim | | 28 | 28 | 0.281 | 80 | 39 | 2 |
| @ Blo | w# | 1 | 1 | 13 | 13 | 1 | 1 |
| | | | Total | number of blows ar | nalyzed: 23 | | |

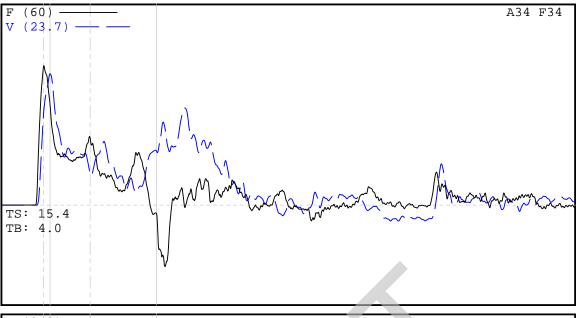
Time Summary

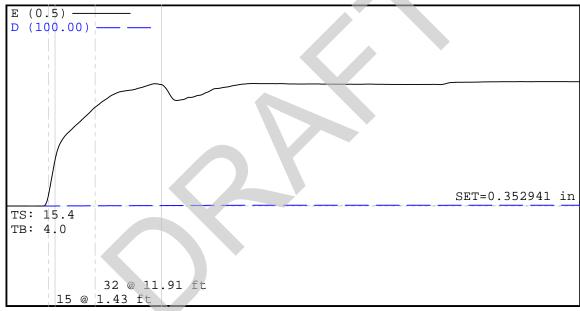
Drive 29 seconds

11:45:13 AM - 11:45:42 AM (9/20/2013) BN 1 - 23

04.55124092

SPT-4 RIG 361982 16FT FUGRO YARD





Project Information

PROJECT: 04.55124092 PILE NAME: SPT-4 RIG 361982 16FT FUGRO YACSI 29.7 ksi

DESCR: SAMPLE 12FT OPERATOR: MAN

FILE: SPT-4 RIG 361982 16FT FUGRO YARD

9/20/2013 12:09:46 PM

Blow Number 12

Pile Properties

LE 23.79 ft AR 1.42 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.5 ksec/ft 2L/C 2.84 ms JC 16.35 ft LP

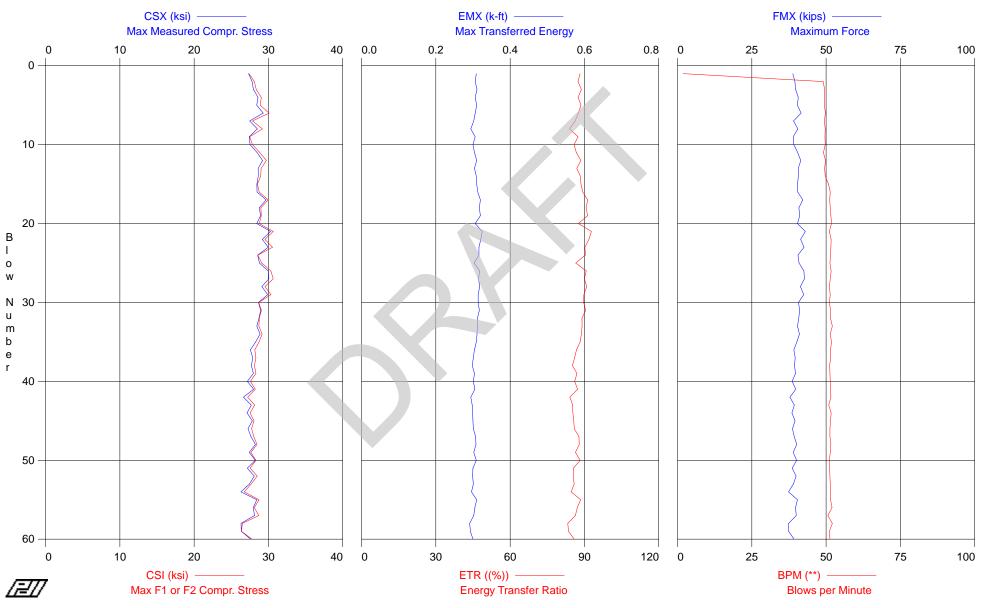
Quantity Results

CSX 29.2 ksi EMX 0.3 k-ft ETR 88.6 (%) FMX 41 kips BPM 49.8 bpm QNV 0.00 [] QNV 0.00 [] QNV 0.00 []

<u>Sensors</u>

F3: [SPT-333NWJ-1] 214 (1) F4: [SPT-333NWJ-2] 213.44 (1) A3: [K1335] 363 mv/5000g's (1) A4: [2286] 342 mv/5000g's (1) CLIP: OK

04.55124092 - SPT-4 RIG 361982 16FT FUGRO YARD



Page 1 of 2 PDIPLOT Ver. 2012.2 - Printed: 25-Sep-2013

SAMPLE 12FT

04.55124092 - SPT-4 RIG 361982 16FT FUGRO YARD

 OP: MAN
 Test date: 20-Sep-2013

 AR: 1.42 in^2
 SP: 0.492 k/ft3

 LE: 23.79 ft
 EM: 30,000 ksi

 WS: 16,807.9 f/s
 JC: 0.00

| | 10,007.91/5 | <u> </u> | | | | | 0.00 |
|------|--|----------|----------|-------|----------|-----------------|-------|
| CSI: | Max Measured Compr. St Max F1 or F2 Compr. St | ress | | | | ETR: Energy Tra | Force |
| | Max Transferred Energy | | | | | BPM: Blows per | |
| BL# | BLC | CSX | CSI | EMX | ETR | FMX | BPM |
| | bl/ft | ksi | ksi | k-ft | (%) | kips | ** |
| 1 | 34 | 27 | 27 | 0.309 | 88 | 39 | 2 |
| 2 | 34 | 28 | 28 | 0.306 | 87 | 39 | 49 |
| 3 | 34 | 28 | 28 | 0.311 | 89 | 40 | 50 |
| 4 | 34 | 29 | 29 | 0.306 | 87 | 41 | 50 |
| 5 | 34 | 28 | 29 | 0.310 | 89 | 40 | 49 |
| 6 | 34 | 29 | 30 | 0.306 | 88 | 42 | 50 |
| 7 | 34 | 27 | 28 | 0.302 | 86 | 39 | 49 |
| 8 | 34 | 29 | 29 | 0.294 | 84 | 40 | 50 |
| 9 | 34 | 27 | 27 | 0.306 | 87 | 39 | 50 |
| 10 | 34 | 28 | 28 | 0.300 | 86 | 39 | 50 |
| 11 | 34 | 28 | 29 | 0.304 | 87 | 40 | 49 |
| 12 | 34 | 29 | 30 | 0.310 | 89 | 41 | 50 |
| 13 | 34 | 29 | 29 | 0.304 | 87 | 41 | 50 |
| 14 | 34 | 29 | 29 | 0.304 | 88 | 41 | 50 |
| 15 | 34 | 28 | 29 | 0.310 | 89 | 40 | 51 |
| | | | | | | | |
| 16 | 34 | 28 | 29 | 0.313 | 89 | 40 | 51 |
| 17 | 34 | 30 | 30 | 0.320 | 91 | 42 | 51 |
| 18 | 42 | 29 | 29 | 0.317 | 91 | 41 | 51 |
| 19 | 42 | 29 | 29 | 0.320 | 91 | 41 | 52 |
| 20 | 42 | 28 | 29 | 0.306 | 88 | 40 | 52 |
| 21 | 42 | 30 | 31 | 0.325 | 93 | 43 | 51 |
| 22 | 42 | 29 | 30 | 0.321 | 92 | 41 | 52 |
| 23 | 42 | 30 | 31 | 0.316 | 90 | 43 | 52 |
| 24 | 42 | 29 | 29 | 0.316 | 90 | 41 | 52 |
| 25 | 42 | 29 | 29 | 0.303 | 86 | 41 | 51 |
| 26 | 42 | 30 | 30 | 0.318 | 91 | 43 | 52 |
| 27 | 42 | 30 | 31 | 0.315 | 90 | 43 | 51 |
| 28 | 42 | 29 | 30 | 0.318 | 91 | 41 | 51 |
| 29 | 42 | 30 | 30 | 0.314 | 90 | 42 | 51 |
| 30 | 42 | 29 | 29 | 0.314 | 90 | 41 | 51 |
| 31 | 42 | 29 | 29 | 0.317 | 91 | 41 | 52 |
| 32 | 42 | 29 | 29 | 0.312 | 89 | 41 | 52 |
| 33 | 42 | 28 | 29 | 0.312 | 89 | 40 | 52 |
| 34 | 42 | 29 | 29 | 0.311 | 89 | 41 | 51 |
| 35 | 42 | 28 | 29 | 0.309 | 88 | 40 | 52 |
| 36 | 42 | 28 | 28 | 0.304 | 87 | 39 | 52 |
| 37 | 42 | 28 | 28 | 0.301 | 86 | 40 | 52 |
| 38 | 42 | 28 | 28 | 0.298 | 85 | 39 | 51 |
| 39 | 48 | 28 | 28 | 0.304 | 87 | 40 | 51 |
| 40 | 48 | 27 | 28 | 0.304 | 86 | 39 | 51 |
| 41 | 48 | 28 | 28 28 | 0.305 | 87 | 40 | 52 |
| | | 27 | 26 27 | | | | |
| 42 | 48 | | | 0.294 | 84 | 38 | 52 |
| 43 | 48 | 28 | 28 | 0.298 | 85 85 | 39 | 51 |
| 44 | 48 | 27 | 28 | 0.299 | 85 | 39 | 52 |
| 45 | 48 | 28 | 28 | 0.300 | 86 | 40 | 52 |
| 46 | 48 | 27 | 28 | 0.301 | 86 | 39 | 51 |
| 47 | 48 | 28 | 28 | 0.307 | 88 | 39 | 51 |
| 48 | 48 | 28 | 28 | 0.308 | 88 | 40 | 52 |
| 49 | 48 | 27 | 28 | 0.302 | 86 | 39 | 51 |
| 50 | 48 | 28 | 28 | 0.309 | 88 | 40 | 51 |
| 51 | 48 | 27 | 28 | 0.300 | 86 | 39 | 51 |
| 52 | 48 | 28 | 29 | 0.299 | 85 | 40 | 51 |
| 53 | 48 | 27 | 28 | 0.301 | 86 | 39 | 51 |
| 54 | 48 | 26 | 27 | 0.296 | 85 | 37 | 51 |
| 55 | 48 | 28 | 29 | 0.310 | 88 | 40 | 52 |
| 56 | 48 | 28 | 28 | 0.305 | 87 | 40 | 52 |
| 57 | 48 | 28 | 29 | 0.302 | 86 | 40 | 51 |
| 58 | 48 | 26 | 26 | 0.291 | 83 | 37 | 52 |
| 59 | 48 | 26 | 26 | 0.293 | 84 | 37 | 51 |
| 60 | 48 | 28 | 28 | 0.300 | 86 | 39 | 51 |
| 61 | 48 | 27 | 27 | 0.298 | 85 | 38 | 52 |
| 62 | 48 | 28 | 28 | 0.307 | 88 | 39 | 52 |
| ~- | | | | | | | ~- |

Page 2 of 2 PDIPLOT Ver. 2012.2 - Printed: 25-Sep-2013

04.55124092 - SPT-4 RIG 361982 16FT FUGRO YARD

SAMPLE 12FT

| OP: MAN | | | | | Test date: 2 | 0-Sep-2013 | |
|-----------|------------------------------------|-----|-------|-----|--------------|------------|--|
| | CSX | CSI | EMX | ETR | FMX | BPM | |
| | ksi | ksi | k-ft | (%) | kips | ** | |
| Average | 28 | 29 | 0.307 | 88 | 40 | 50 | |
| Std. Dev. | 1 | 1 | 0.008 | 2 | 1 | 6 | |
| Maximum | 30 | 31 | 0.325 | 93 | 43 | 52 | |
| @ Blow# | 21 | 21 | 21 | 21 | 21 | 33 | |
| Minimum | 26 | 26 | 0.291 | 83 | 37 | 2 | |
| @ Blow# | 54 | 59 | 58 | 58 | 54 | 1 | |
| | Total number of blows analyzed: 62 | | | | | | |

Time Summary

Drive 1 minute 11 seconds 12:09:33 PM - 12:10:44 PM (9/20/2013) BN 1 - 62





11955 Lakeland Park Blvd. Ste. 100 Baton Rouge, Louisiana 70809 225.293.2460

January 13, 2014

HDR Engineering, Inc. 2365 Iron Point Road, Suite 300 Folsom, CA 95630

Attention: Mr. Mark Stanley, GE

Senior Geotechnical Advisor

Subject: Letter Report

SPT Energy Measurement

Cathead-Operated Safety Hammer on Marsh Buggy #23 Drill Rig State of Louisiana Coastal Protection and Restoration Authority

Mid Barataria Diversion (BA-153) Project

Plaquemines Parish, Louisiana File No. 18274-001-00, Task 0300

GeoEngineers, Inc. (GeoEngineers) recently completed the standard penetration test (SPT) energy measurement testing on the cathead operated safety hammer of the Marsh Buggy #23 drill rig. The drill rig is owned and operated by Specialized Environmental Resources (SER).

Measurements were made January 10, 2014 by Ivy A. Harmon, a GeoEngineers staff engineer, using a Pile Dynamic Analyzer (PDA) model PAX and a calibrated, instrumented drill rod. The energy testing was completed between 27.5 and 39 feet below the ground surface. Measurements were recorded at four depth intervals; this report includes results from three depth intervals. The unused depth interval was determined to not provide representative test data.

The drill rig used was a pontoon-tracked marsh buggy, SER #23, hull identification MBD#01 WWC-709. The driller was Johnny Gallow, and John Francis was the drilling assistant. The hammer was a CME-style cathead-driven safety hammer in good condition. The 1-inch diameter rope was in good condition, and was wrapped 1 turn around the cathead. The drill rod used is proprietary to SER and is light-weight shothole casing type rod. The SPT procedures were conducted in general accordance with ASTM D-1586-08-a. GeoEngineers observed that the driller was hesitant when performing the initial SPT operations due to the presence of instrumentation, but as he gained confidence in the testing equipment the procedure continued normally. The hesitation during the first test made the record unusable as a measurement of the SPT energy.

A summary of the energy measurement results is included in the table below for selected test intervals between 27.5 and 39 feet below the ground surface. Based on the collected data, the overall average energy measured in the drill pipe was about 58% of the expected SPT hammer energy.

SPT HAMMER ENERGY MEASUREMENT RESULTS

| Depth Increment (ft) | Cathead/Hammer Operator | Average Energy Transfer Ratio (%) | Penetration Resistance (Blows/ft) |
|----------------------------|----------------------------|---|-----------------------------------|
| 27.5 to 29 | J. Gallow | 53.5 | 24 |
| 30 to 31.5 | J. Gallow | 57.3 | 15 |
| 37.5 to 39 | J. Gallow | 62.4 | 20 |

Measurement details are available in the attached PDA output reports, including an example Force-Velocity-Time graph generated may a single sample blow at each test increment.

We appreciate the opportunity to work with HDR on this project. Please call up at 225.293.2460 if you have any comments or questions.

Sincerely,

GeoEngineers, Inc.

Wy A. Harmon, E.I.

Staff Geotechnical Engineer

er S. Custer Charles L. Eustis, P.E.

Principal

Appendix A. SPT Energy Measurement Reports

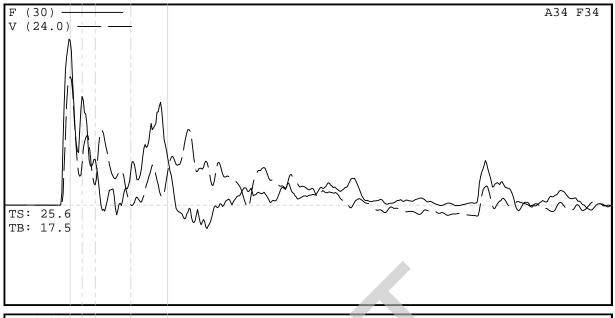
Disclaimer: Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.

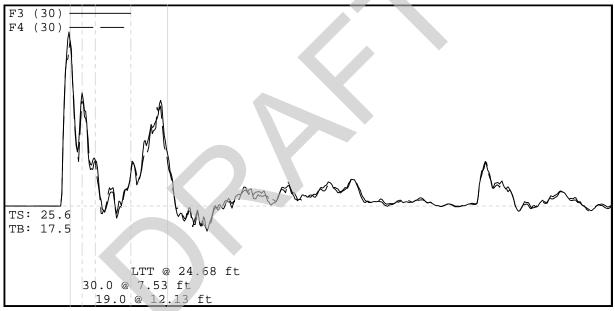
Confidential Information: Privileged and Confidential Work Product.

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MID BARATARIA CALIBRATION

SER MARSH BUGGY, 27.5-29





Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: SER MARSH BUGGY, 27.5-29 DESCR: SPT ENERGY MEASURE

ODEDATOD: IAII

OPERATOR: IAH

FILE: SER MARSH BUGGY, TEST 2.W01

1/10/2014 9:22:00 AM

Blow Number 27

Pile Properties

LE 34.30 ft AR 0.70 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 1.2 ksec/ft 2L/C 4.10 ms JC 0.90 [] LP 28.62 ft

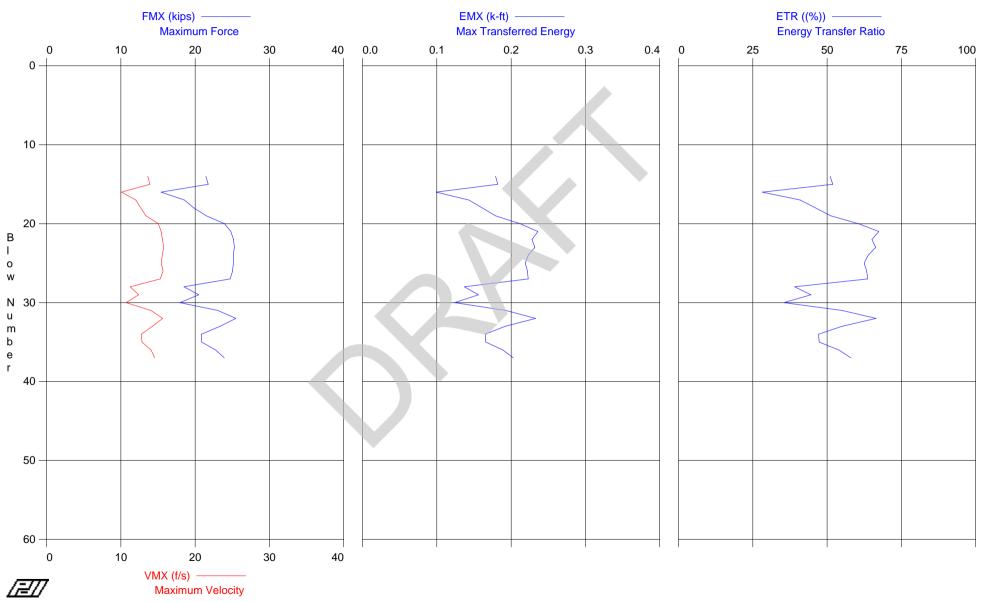
Quantity Results

FMX 25 kips VMX 15.3 f/s DMX 0.53 in EMX 0.22 k-ft CSX 35.30 ksi CSI 37.02 ksi BTA 19.0 (%) RX9 4 kips BPM 15.4 bpm

Sensors

F3: [402SW-1] 210.62 (1) F4: [402SW-2] 204.74 (1) A3: [K1578] 325 mv/5000g's (1) A4: [K1580] 355 mv/5000g's (1) CLIP: OK

MID BARATARIA CALIBRATION - SER MARSH BUGGY, 27.5-29



Page 1 of 1

PDIPLOT Ver. 2014.1 - Printed: 13-Jan-2014

SPT ENERGY MEASURE

MID BARATARIA CALIBRATION - SER MARSH BUGGY, 27.5-29 OP: IAH Test date: 10-Jan-2014

AR: 0.70 in^2 SP: 0.492 k/ft3 LE: 34.30 ft EM: 30,000 ksi WS: 16,807.9 f/s JC: 0.90

FMX: Maximum Force CSX: Max Measured Compr. Stress VMX: Maximum Velocity

BTA: BETA Integrity Factor
RX9: Max Case Method Capacity (JC=0.9) DMX: Maximum Displacement

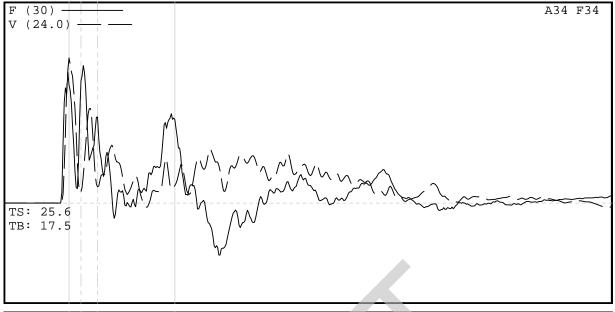
| EMX: Max Transferred Energy | | | | | | BPM: Blows per Minute | | | | | |
|-----------------------------|------------------------------------|-------------|------|------|------|-----------------------|------|-------|------|------|------|
| ETR: | Energy Trai | nsfer Ratio | | | | | | | | | |
| BL# | depth | BLC | FMX | VMX | DMX | EMX | ETR | CSX | BTA | RX9 | BPM |
| | · ft | bl/ft | kips | f/s | in | k-ft | (%) | ksi | (%) | kips | ** |
| 14 | 28.05 | 22 | 21 | 13.6 | 0.59 | 0.18 | 51.0 | 30.64 | 20.0 | · 4 | 35.0 |
| 15 | 28.09 | 22 | 22 | 13.9 | 0.58 | 0.18 | 51.9 | 31.10 | 21.0 | 4 | 35.0 |
| 16 | 28.14 | 22 | 15 | 10.1 | 0.55 | 0.10 | 28.2 | 22.01 | 16.0 | 5 | 32.6 |
| 17 | 28.18 | 22 | 19 | 12.0 | 0.55 | 0.14 | 40.9 | 26.50 | 22.0 | 5 | 35.9 |
| 18 | 28.23 | 22 | 20 | 12.7 | 0.55 | 0.16 | 46.1 | 28.32 | 21.0 | 5 | 34.3 |
| 19 | 28.27 | 22 | 22 | 13.4 | 0.55 | 0.18 | 51.2 | 30.74 | 24.0 | 5 | 34.2 |
| 20 | 28.32 | 22 | 24 | 15.0 | 0.57 | 0.21 | 60.5 | 34.22 | 23.0 | 5 | 35.1 |
| 21 | 28.36 | 22 | 25 | 15.4 | 0.62 | 0.24 | 67.4 | 35.44 | 23.0 | 5 | 34.8 |
| 22 | 28.41 | 22 | 25 | 15.6 | 0.57 | 0.23 | 65.1 | 35.97 | 14.0 | 4 | 35.3 |
| 23 | 28.45 | 22 | 25 | 15.8 | 0.58 | 0.23 | 66.3 | 36.12 | 17.0 | 5 | 34.2 |
| 24 | 28.50 | 22 | 25 | 15.6 | 0.55 | 0.22 | 63.8 | 35.90 | 16.0 | 3 | 35.6 |
| 25 | 28.54 | 26 | 25 | 15.4 | 0.51 | 0.22 | 62.5 | 35.91 | 15.0 | 4 | 35.9 |
| 26 | 28.58 | 26 | 25 | 15.7 | 0.53 | 0.22 | 63.3 | 35.78 | 17.0 | 4 | 35.2 |
| 27 | 28.62 | 26 | 25 | 15.3 | 0.53 | 0.22 | 63.6 | 35.30 | 19.0 | 4 | 15.4 |
| 28 | 28.65 | 26 | 18 | 11.3 | 0.46 | 0.14 | 39.1 | 26.42 | 23.0 | 6 | 35.2 |
| 29 | 28.69 | 26 | 20 | 12.4 | 0.46 | 0.16 | 44.6 | 29.28 | 24.0 | 4 | 26.5 |
| 30 | 28.73 | 26 | 18 | 10.7 | 0.46 | 0.12 | 35.4 | 25.61 | 24.0 | 4 | 29.5 |
| 31 | 28.77 | 26 | 23 | 14.1 | 0.46 | 0.19 | 55.1 | 32.94 | 23.0 | 4 | 35.7 |
| 32 | 28.81 | 26 | 25 | 15.6 | 0.53 | 0.23 | 66.5 | 36.41 | 21.0 | 4 | 30.9 |
| 33 | 28.85 | 26 | 23 | 14.2 | 0.46 | 0.19 | 55.0 | 33.34 | 17.0 | 5 | 14.4 |
| 34 | 28.88 | 26 | 21 | 12.8 | 0.46 | 0.17 | 47.1 | 29.79 | 20.0 | 5 | 33.0 |
| 35 | 28.92 | 26 | 21 | 12.8 | 0.46 | 0.17 | 47.3 | 29.83 | 27.0 | 4 | 34.7 |
| 36 | 28.96 | 26 | 23 | 14.1 | 0.46 | 0.19 | 54.0 | 32.53 | 22.0 | 5 | 33.3 |
| 37 | 29.00 | 26 | 24 | 14.6 | 0.46 | 0.20 | 58.0 | 34.16 | 22.0 | 4 | 33.7 |
| | | Average | 22 | 13.8 | 0.52 | 0.19 | 53.5 | 31.84 | 20.5 | 4 | 32.3 |
| | | Std. Dev. | 3 | 1.7 | 0.05 | 0.04 | 10.6 | 3.92 | 3.3 | 1 | 5.7 |
| | | Maximum | 25 | 15.8 | 0.62 | 0.24 | 67.4 | 36.41 | 27.0 | 6 | 35.9 |
| | | @ Blow# | 32 | 23 | 21 | 21 | 21 | 32 | 35 | 28 | 17 |
| | Total number of blows analyzed: 24 | | | | | | | | | | |

Time Summary

Drive 1 minute 13 seconds 9:21:08 AM - 9:22:21 AM (1/10/2014) BN 1 - 37

MID BARATARIA CALIBRATION

SER MARSH BUGGY, 30-31.5





Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: SER MARSH BUGGY, 30-31.5 DESCR: SPT ENERGY MEASURE

OPERATOR: IAH

FILE: SER MARSH BUGGY, TEST 3.W01

1/10/2014 9:41:29 AM

Blow Number 15

Pile Properties

LE 37.30 ft AR 0.70 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 1.2 ksec/ft 2L/C 4.46 ms JC 0.90 [] LP 31.28 ft

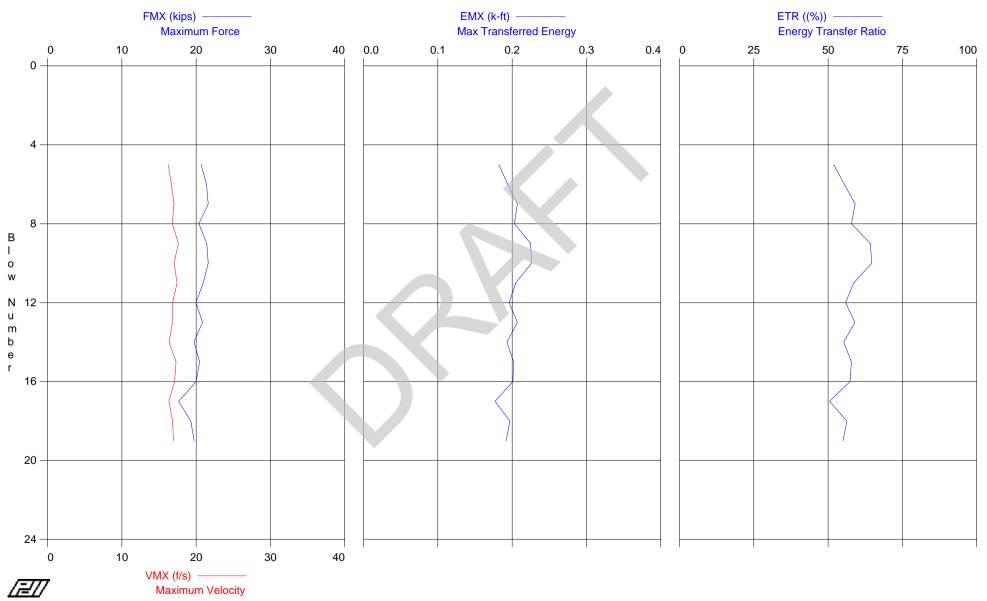
Quantity Results

FMX 20 kips VMX 17.3 f/s DMX 0.71 in EMX 0.20 k-ft CSX 29.23 ksi CSI 30.66 ksi BTA 0.0 (%) RX9 11 kips BPM 36.5 bpm

Sensors

F3: [402SW-1] 210.62 (1) F4: [402SW-2] 204.74 (1) A3: [K1578] 325 mv/5000g's (1) A4: [K1580] 355 mv/5000g's (1) CLIP: OK

MID BARATARIA CALIBRATION - SER MARSH BUGGY, 30-31.5



MID BARATARIA CALIBRATION - SER MARSH BUGGY, 30-31.5

Page 1 of 1

PDIPLOT Ver. 2014.1 - Printed: 13-Jan-2014

SPT ENERGY MEASURE Test date: 10-Jan-2014

AR: 0.70 in^2 SP: 0.492 k/ft3 LE: 37.30 ft EM: 30,000 ksi WS: 16,807.9 f/s JC: 0.90

FMX: Maximum Force CSX: Max Measured Compr. Stress VMX: Maximum Velocity BTA: **BETA Integrity Factor**

DMX: Maximum Displacement RX9: Max Case Method Capacity (JC=0.9)

BPM: Blows per Minute EMX: Max Transferred Energy ETR: Energy Transfer Ratio **FMX** VMX DMX **EMX ETR** RX9 BPM BL# depth CSX **BTA** bl/ft kips f/s k-ft (%) ksi (%) kips 5 30.58 12 21 16.2 1.07 0.18 51.9 29.52 0.0 12 24.3 6 12 21 16.7 55.5 30.56 29.0 30.67 1.08 0.19 0.0 6 1.08 30.75 12 22 59.1 30.90 10 32.3 7 17.0 0.21 0.0 8 12 20 57.9 29.10 30.83 16.8 1.04 0.20 0.0 11 28.8 9 30.92 12 21 17.6 1.02 0.23 64.2 30.62 0.0 10 29.6 10 31.00 12 22 17.0 1.01 0.23 64.7 30.89 0.0 4 31.0 0.21 13 11 31.06 18 21 17.4 0.79 58.6 29.94 0.0 30.7 12 10 32.0 18 20 16.8 0.75 0.20 55.9 28.53 0.0 31.11 21 29.81 13 31.17 18 16.8 0.75 0.21 59.0 0.0 9 32.2 14 31.22 18 20 16.3 0.73 0.19 55.2 28.15 0.0 15 34.2 15 31.28 18 20 17.3 0.71 0.20 57.8 29.23 0.0 36.5 11 35.5 16 31.33 18 20 17.1 0.73 0.20 57.4 28.58 0.0 11 17 31.39 18 18 0.18 50.5 25.22 0.0 9 32.1 16.3 0.67 18 31.44 18 19 16.8 0.67 0.20 56.3 27.54 0.0 11 39.8 19 31.50 18 20 16.9 0.67 0.19 55.0 28.19 0.0 15 36.8

0.85

Std. Dev. 1 0.4 0.17 0.01 3.7 1.46 0.0 3 3.7 Maximum 22 17.6 1.08 0.23 64.7 30.90 15 39.8 0.0 @ Blow# 10 10 5 19 18 6

57.3

29.12

0.0

10

32.3

Total number of blows analyzed: 15

0.20

Time Summary

Average

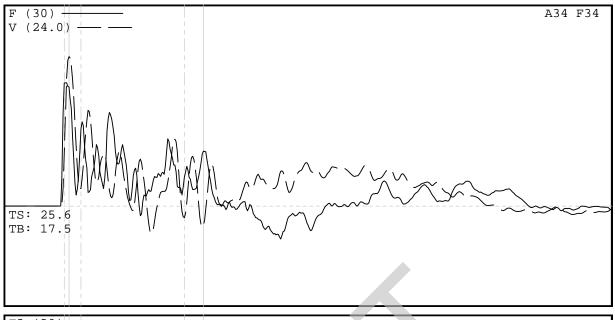
20

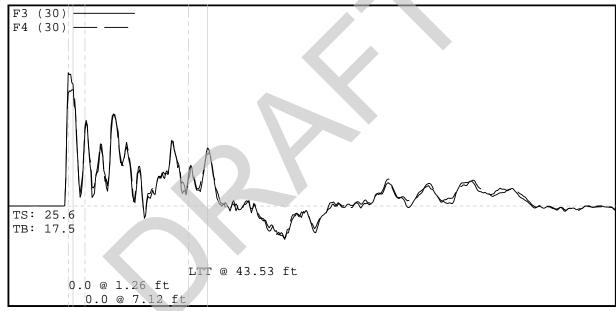
Drive 35 seconds 9:41:02 AM - 9:41:37 AM (1/10/2014) BN 1 - 19

16.9

MID BARATARIA CALIBRATION

SER MARSH BUGGY, 37.5-39





Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: SER MARSH BUGGY, 37.5-39

DESCR: SPT ENERGY MEASURE

OPERATOR: IAH

FILE: SER MARSH BUGGY, TEST 5_1.W01

1/10/2014 10:12:11 AM

Blow Number 13

Pile Properties

LE 47.30 ft AR 0.70 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 1.2 ksec/ft 2L/C 5.65 ms JC 0.90 [] LP 38.33 ft

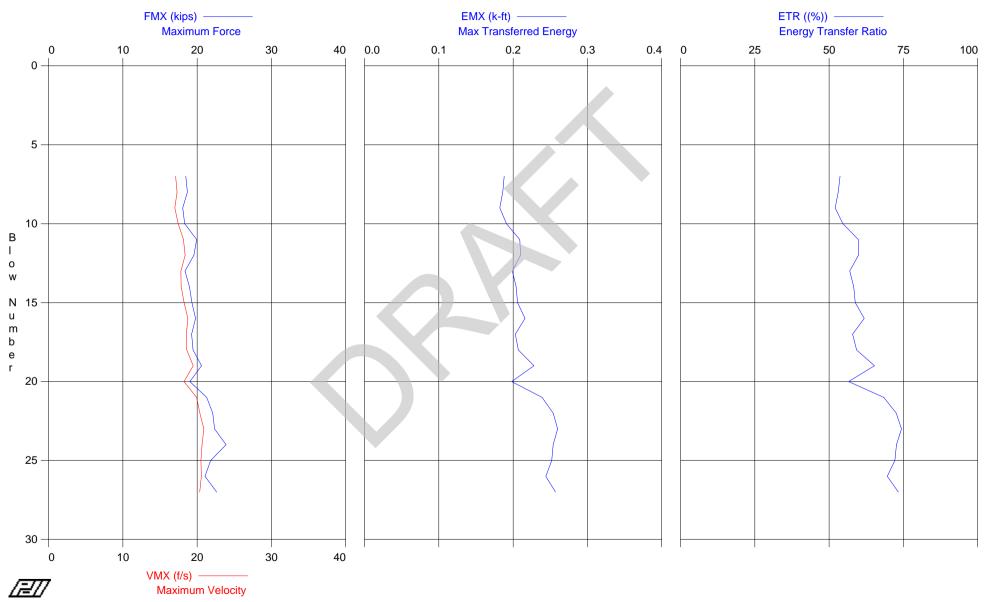
Quantity Results

FMX 18 kips VMX 17.8 f/s DMX 0.68 in EMX 0.20 k-ft CSX 26.22 ksi CSI 28.35 ksi BTA 0.0 (%) RX9 13 kips BPM 37.7 bpm

<u>Sensors</u>

F3: [402SW-1] 210.62 (1) F4: [402SW-2] 204.74 (1) A3: [K1578] 325 mv/5000g's (1) A4: [K1580] 355 mv/5000g's (1) CLIP: OK

MID BARATARIA CALIBRATION - SER MARSH BUGGY, 37.5-39



Page 1 of 1

PDIPLOT Ver. 2014.1 - Printed: 13-Jan-2014

MID BARATARIA CALIBRATION - SER MARSH BUGGY, 37.5-39

SPT ENERGY MEASURE

| OP: I | AH | lest date: 10-Jar | 1-2014 |
|-------|--------------|-------------------|----------------|
| AR: | 0.70 in^2 | SP: 0.49 | 92 k/ft3 |
| LE: | 47.30 ft | EM: 30,00 |)0 ksi |
| WS: | 16,807.9 f/s | JC: 0.9 |) 0 |
| | | | |

FMX: Maximum Force VMX: Maximum Velocity

CSX: Max Measured Compr. Stress BTA: BETA Integrity Factor RX9: Max Case Method Capacity (JC=0.9) DMX: Maximum Displacement

| EMX: Max Transferred Energy | | | | | | | BPM: Blows per Minute | | | | | |
|-----------------------------|-------|--------------|------|------|------|------|-----------------------|-------|----------|------|------|--|
| ETR: | | ansfer Ratio | | | | | | 2 2.0 | o po:a.o | | | |
| BL# | depth | BLC | FMX | VMX | DMX | EMX | ETR | CSX | BTA | RX9 | BPM | |
| | · ft | bl/ft | kips | f/s | in | k-ft | (%) | ksi | (%) | kips | ** | |
| 7 | 38.00 | 14 | 18 | 17.1 | 0.86 | 0.19 | 53.7 | 26.38 | 0.0 | 12 | 35.0 | |
| 8 | 38.06 | 18 | 19 | 17.3 | 0.68 | 0.19 | 53.1 | 26.69 | 0.0 | 13 | 35.5 | |
| 9 | 38.11 | 18 | 18 | 17.0 | 0.67 | 0.18 | 52.0 | 25.81 | 0.0 | 11 | 35.6 | |
| 10 | 38.17 | 18 | 18 | 17.4 | 0.70 | 0.19 | 54.6 | 26.16 | 0.0 | 13 | 37.0 | |
| 11 | 38.22 | 18 | 20 | 18.2 | 0.72 | 0.21 | 59.8 | 28.48 | 0.0 | 13 | 36.9 | |
| 12 | 38.28 | 18 | 20 | 18.4 | 0.67 | 0.21 | 59.9 | 27.93 | 0.0 | 12 | 36.2 | |
| 13 | 38.33 | 18 | 18 | 17.8 | 0.68 | 0.20 | 57.0 | 26.23 | 0.0 | 13 | 37.7 | |
| 14 | 38.39 | 18 | 19 | 17.8 | 0.67 | 0.20 | 58.3 | 27.10 | 9.0 | 8 | 36.8 | |
| 15 | 38.44 | 18 | 19 | 18.2 | 0.68 | 0.21 | 58.8 | 27.57 | 5.0 | 14 | 37.4 | |
| 16 | 38.50 | 18 | 20 | 18.8 | 0.67 | 0.22 | 61.8 | 28.27 | 1.0 | 14 | 36.8 | |
| 17 | 38.55 | 22 | 19 | 18.5 | 0.61 | 0.20 | 57.9 | 27.51 | 1.0 | 14 | 35.8 | |
| 18 | 38.59 | 22 | 19 | 18.6 | 0.57 | 0.21 | 59.3 | 27.78 | 4.0 | 11 | 36.7 | |
| 19 | 38.64 | 22 | 21 | 19.5 | 0.66 | 0.23 | 65.3 | 29.43 | 3.0 | 16 | 37.2 | |
| 20 | 38.68 | 22 | 19 | 18.2 | 0.57 | 0.20 | 56.6 | 27.18 | 3.0 | 11 | 36.0 | |
| 21 | 38.73 | 22 | 21 | 19.9 | 0.68 | 0.24 | 68.4 | 30.41 | 0.0 | 17 | 35.3 | |
| 22 | 38.77 | 22 | 22 | 20.4 | 0.67 | 0.25 | 72.6 | 31.58 | 1.0 | 15 | 36.4 | |
| 23 | 38.82 | 22 | 22 | 20.9 | 0.70 | 0.26 | 74.4 | 31.92 | 4.0 | 17 | 36.7 | |
| 24 | 38.86 | 22 | 24 | 20.7 | 0.70 | 0.25 | 72.7 | 34.13 | 0.0 | 14 | 37.4 | |
| 25 | 38.91 | 22 | 22 | 20.5 | 0.62 | 0.25 | 72.1 | 31.18 | 0.0 | 13 | 34.7 | |
| 26 | 38.95 | 22 | 21 | 20.6 | 0.65 | 0.24 | 69.6 | 30.08 | 2.0 | 15 | 37.1 | |
| 27 | 39.00 | 22 | 23 | 20.3 | 0.62 | 0.26 | 73.3 | 32.32 | 0.0 | 14 | 37.7 | |
| | | Average | 20 | 18.9 | 0.67 | 0.22 | 62.4 | 28.77 | 1.6 | 13 | 36.5 | |
| | | Std. Dev. | 2 | 1.3 | 0.06 | 0.03 | 7.3 | 2.31 | 2.3 | 2 | 0.9 | |
| | | Maximum | 24 | 20.9 | 0.86 | 0.26 | 74.4 | 34.13 | 9.0 | 17 | 37.7 | |
| | | @ Blow# | 24 | 23 | 7 | 23 | 23 | 24 | 14 | 21 | 13 | |

23 23 Total number of blows analyzed: 21

Time Summary

Drive 44 seconds 10:11:51 AM - 10:12:35 AM (1/10/2014) BN 1 - 27



11955 Lakeland Park Blvd, Suite 100 Baton Rouge, Louisiana 70809 225.293.2460

August 1, 2013

HDR Engineering, Inc. 2365 Iron Point Road, Suite 300 Folsom, CA 95630

Attention: Mr. Mark Stanley, GE

Senior Geotechnical Advisor

Subject: Letter Report

SPT Energy Measurement

Cathead-Operated Safety Hammer on Failing 1500 Drill Rig State of Louisiana Coastal Protection and Restoration Authority

Mid Barataria Diversion (BA-153) Project

Plaquemines Parish, LA

File No. 18274-001-00, Task 0300

GeoEngineers, Inc. (GeoEngineers) is sending this document to report on the recent standard penetration test (SPT) energy measurement testing we completed on the Failing 1500 drill rig with the cathead-operated safety hammer. Testing was completed prior to mobilizing the drilling equipment to the project site in Plaquemines Parish, Louisiana.

Measurements were made by Ivy A. Harmon, a GeoEngineers staff engineer, using a PDA model PAX and a calibrated, instrumented drill rod. The energy testing was completed between 25 and 34.5 feet below the ground surface. Measurements were taken at three depth intervals; this report includes results from the each depth interval.

The drill rig used was a truck-mounted Failing 1500 Drill Rig, GeoEngineers Rig 49. The hammer was a CME-style cathead-driven safety hammer in good condition. In general, the rope was in very good condition (a nearly new, 1-inch diameter rope was used). The rope was typically wrapped 2 ¼ turns around the cathead. The SPT procedures were conducted in general accordance with ASTM D1586-08a. We observed that the driller was hesitant when performing initial STP operations due to the presence of instrumentation, but as he gained confidence in the testing equipment the procedure continued normally.

A summary of the energy measurement results is included in the table below for selected increments between 25 and 34.5 feet below the ground surface. Based on the collected data (see the table below), the overall average energy measured in the drill pipe was about 72% of the expected SPT hammer energy.

SPT HAMMER ENERGY MEASUREMENT RESULTS

| Depth increment (ft) | Cathead/Hammer Operator | Average Energy Transfer Ratio (%) | Penetration Resistance (Blows/ft) |
|-------------------------|----------------------------|--|---|
| 25 to 26.5 | R. Clark | 56.4 | 6 |
| 30 to 31.5 | R. Clark | 80.3 | 39 |
| 33 to 34.5 | R. Clark | 78.2 | 36 |

Measurement details are available in the attached PDA output reports, including an example Force-Velocity-Time graph generated by a single sample blow at each depth.

We appreciate the opportunity to work with HDR Engineering, Inc. on this project. Please call us at 225.293.2460 if you have any comments and questions.

Sincerely,

GeoEngineers, Inc.

Ivy A. Harmon, E.I.

Staff Geotechnical Engineer

Charles L. Eustis, P.E.

Principal

Appendix A. SPT Energy Measurement Reports

Disclaimer: Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.

Confidential Information: Privileged and Confidential Work Product.

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11955 Lakeland Park Blvd, Suite 100 Baton Rouge, Louisiana 70809 225.293.2460

APPENDIX A SPT Energy Measurement Reports

MID BARATARIA CALIBRATION - BLUE FAILING TEST 1 SPT NRG MEAS. 1

| MID DANATANIA CALIDINATION - DECET AILING TEST T | SI I NICO MEAS. I |
|--|--|
| OP: IAH | Test date: 21-Jun-2013 |
| AR: 2.36 in^2 | SP: 0.492 k/ft3 |
| LE: 32.00 ft | EM: 30,000 ksi |
| WS: 16,807.9 f/s | JC: 0.35 |
| FMX: Maximum Force | EMX: Max Transferred Energy |
| VMX: Maximum Velocity | ETR: Energy Transfer Ratio |
| DMX: Maximum Displacement | RX6: Max Case Method Capacity (JC=0.6) |
| BPM: Blows per Minute | LTD: Length to Damage |
| EFV: Energy of FV | |

Statistics for entire file (15 blows)

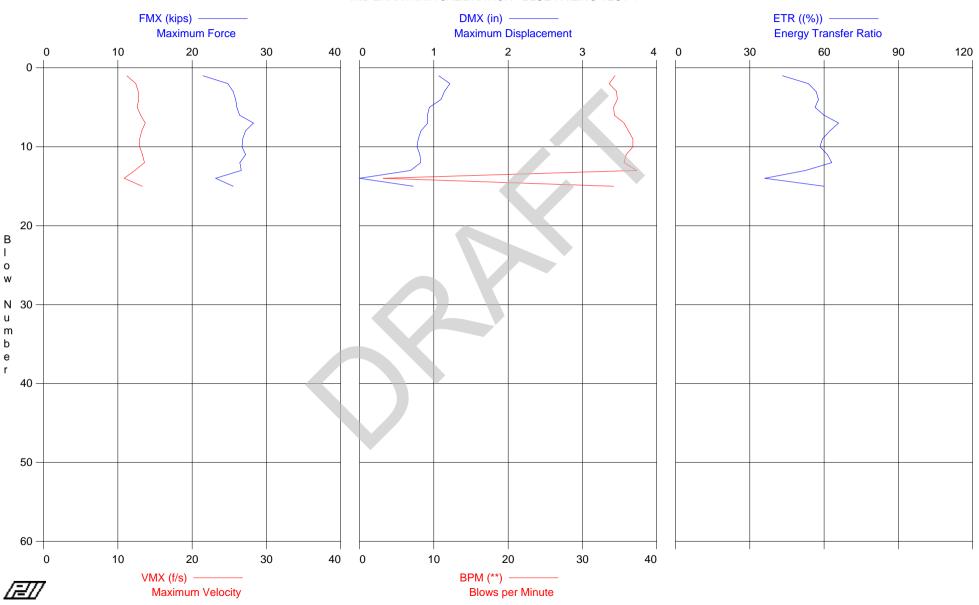
| dodoo for critic in | c (10 blows) | | | | | | | | |
|---------------------|--------------|------|------|------|------|------|------|------|-------|
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft |
| Average | 26 | 12.7 | 0.85 | 33.2 | 0.20 | 0.20 | 56.4 | 15 | 9.67 |
| Std. Dev. | 2 | 0.8 | 0.27 | 8.1 | 0.03 | 0.03 | 7.5 | 4 | 5.27 |
| Maximum | 28 | 13.7 | 1.22 | 37.3 | 0.23 | 0.23 | 65.8 | 17 | 12.99 |
| @ Blow# | 7 | 7 | 2 | 13 | 7 | 7 | 7 | 15 | 1 |

Time Summary

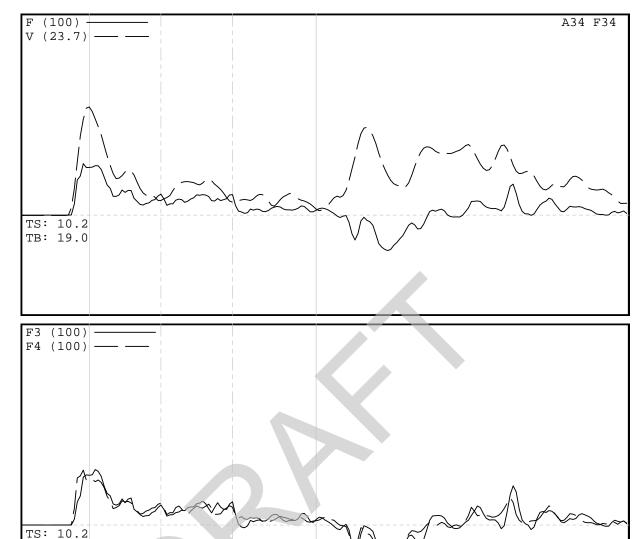
11:32:40 AM - 11:33:20 AM (6/21/2013) BN 1 - 15 Drive 40 seconds

Test date: 21-Jun-2013

MID BARATARIA CALIBRATION - BLUE FAILING TEST 1



BLUE FAILING TEST 1



Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: BLUE FAILING TEST 1

DESCR: SPT NRG MEAS. 1

OPERATOR: IAH

TB: 19.0

FILE: BLUE FAILING TEST 1.W01

6/21/2013 11:32:43 AM

Blow Number 3

Pile Properties

LP

LE 32.00 ft
AR 2.36 in^2
EM 30000 ksi
SP 0.492 k/ft3
WS 16807.9 f/s
EA/C 4.2 ksec/ft
2L/C 3.82 ms
JC 0.35 []

25.00 ft

Quantity Results

73 @ 22.63 ft

73 @ 12.57 ft

FMX 26 kips VMX 12.7 f/s DMX 1.14 in BPM 34.6 bpm EFV 0.20 k-ft EMX 0.20 k-ft ETR 56.8 (%) RX6 16 kips LTD 12.57 ft

Sensors

F3: [151 N3-1] 215.1 (1) F4: [151 N3-2] 216.74 (1) A3: [K1580] 355 mv/5000g's (1) A4: [K1578] 325 mv/5000g's (1) CLIP: OK

| MID BARATARIA | CALIBRATION - | BLUE FAILING | TEST 2 |
|---------------|----------------------|---------------------|--------|
| OD 1411 | | | |

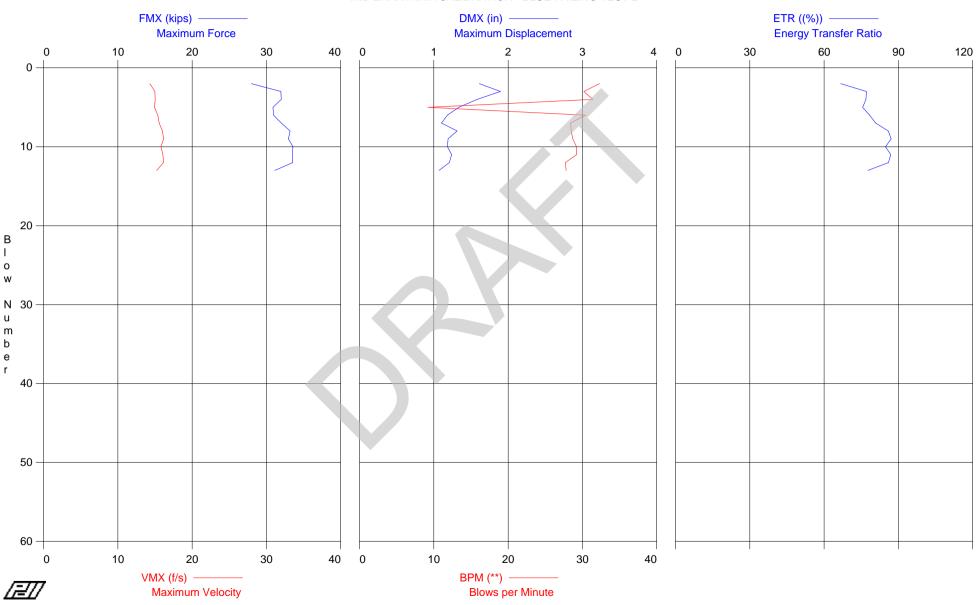
| MID BARATARIA CALIBRATION - BLUE FAILING TEST 2 | | | | | | | | SPT NR | G MEAS. 2 | |
|---|--------------|------|------|------|------|---------|--|--------------|-------------|--|
| OP: IAH | | | | | | | Т | est date: 21 | I-Jun-2013 | |
| AR: 2.36 in^2 | | | | | | | | SP: | 0.492 k/ft3 | |
| LE: 34.00 ft | | | | | | | | EM: 3 | 0,000 ksi | |
| WS: 16,807.9 f/s | | | | | | | | JC: | 0.35 | |
| FMX: Maximum Ford | ce | | | | | EMX: M | ax Transferre | ed Energy | | |
| VMX: Maximum Velo | city | | | | | ETR: E | nergy Transfe | er Ratio | | |
| DMX: Maximum Disp | lacement | | | | | RX6: M | RX6: Max Case Method Capacity (JC=0.6) | | | |
| BPM: Blows per Mini | ute | | | | | LTD: Le | ength to Dam | age | | |
| EFV: Energy of FV | | | | | | | | | | |
| Statistics for entire file | e (12 blows) | | | | | | | | | |
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD | |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft | |
| Average | 32 | 15.5 | 1.33 | 27.8 | 0.28 | 0.28 | 80.3 | 23 | 1.73 | |
| Std. Dev. | 2 | 0.6 | 0.24 | 5.8 | 0.02 | 0.02 | 5.9 | 3 | 1.61 | |
| Maximum | 34 | 16.2 | 1.90 | 32.3 | 0.31 | 0.31 | 87.1 | 26 | 7.07 | |
| @ Blow# | 10 | 9 | 3 | 2 | 9 | 9 | 9 | 12 | 13 | |

Time Summary

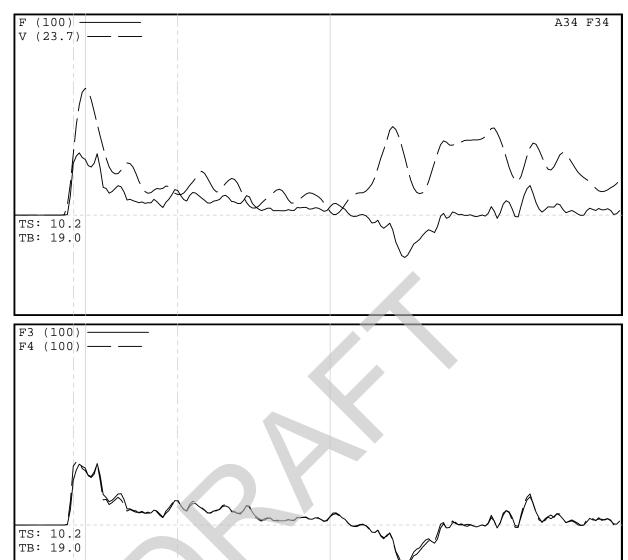
11:53:12 AM - 11:53:41 AM (6/21/2013) BN 1 - 13 Drive 29 seconds

Test date: 21-Jun-2013

MID BARATARIA CALIBRATION - BLUE FAILING TEST 2



BLUE FAILING TEST 2



Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: BLUE FAILING TEST 2 DESCR: SPT NRG MEAS. 2

51 @ 1.25 ft

OPERATOR: IAH

FILE: BLUE FAILING TEST 2.W01

6/21/2013 11:53:23 AM

Blow Number 5

Pile Properties

LE 34.00 ft AR 2.36 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 4.2 ksec/ft 2L/C 4.09 ms JC 0.35 [] LP 30.00 ft

Quantity Results

74 @ 15.79 ft

FMX 31 kips VMX 14.9 f/s DMX 1.34 in BPM 9.2 bpm EFV 0.26 k-ft EMX 0.26 k-ft ETR 75.6 (%) RX6 21 kips LTD 1.25 ft

Sensors

F3: [151 N3-1] 215.1 (1) F4: [151 N3-2] 216.74 (1) A3: [K1580] 355 mv/5000g's (1) A4: [K1578] 325 mv/5000g's (1) CLIP: OK

Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 21-Jun-2013

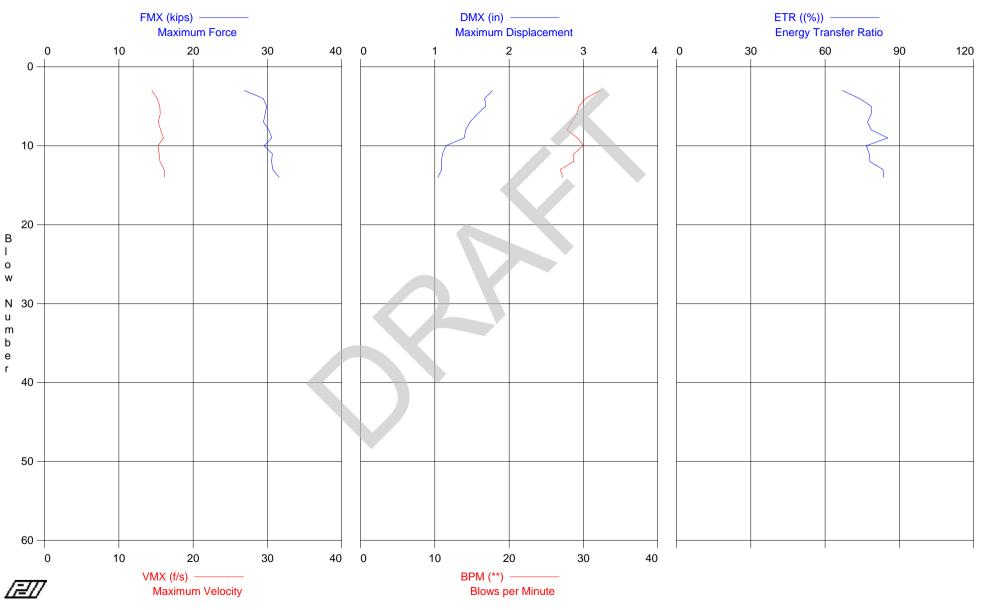
| MID BARATARIA | CALIBRATION - | BLUE FAILING | TEST 3 |
|---------------|---------------|---------------------|--------|
| 00 1411 | | | |

| MID BARATARIA CALIBRATION - BLUE FAILING TEST 3 | | | | | | | | SPT NR | G MEAS. 3 | |
|---|--------------|------|------|------|------|---------|--|--------------|-------------|--|
| OP: IAH | | | | | | | Т | est date: 21 | I-Jun-2013 | |
| AR: 2.36 in^2 | | | | | | | | SP: | 0.492 k/ft3 | |
| LE: 37.00 ft | | | | | | | | EM: 3 | 0,000 ksi | |
| WS: 16,807.9 f/s | | | | | | | | JC: | 0.35 | |
| FMX: Maximum Ford | e | | | | | EMX: M | ax Transferre | ed Energy | | |
| VMX: Maximum Velo | city | | | | | ETR: E | nergy Transfe | er Ratio | | |
| DMX: Maximum Disp | lacement | | | | | RX6: M | RX6: Max Case Method Capacity (JC=0.6) | | | |
| BPM: Blows per Min | ute | | | | | LTD: Le | ength to Dam | age | | |
| EFV: Energy of FV | | | | | | | | | | |
| Statistics for entire file | e (12 blows) | | | | | | | | | |
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD | |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft | |
| Average | 30 | 15.5 | 1.37 | 29.0 | 0.27 | 0.27 | 78.2 | 25 | 5.18 | |
| Std. Dev. | 1 | 0.4 | 0.26 | 1.4 | 0.02 | 0.02 | 4.6 | 1 | 2.77 | |
| Maximum | 32 | 16.2 | 1.78 | 32.2 | 0.30 | 0.30 | 85.3 | 27 | 7.14 | |
| @ Blow# | 14 | 14 | 3 | 3 | 9 | 9 | 9 | 9 | 3 | |

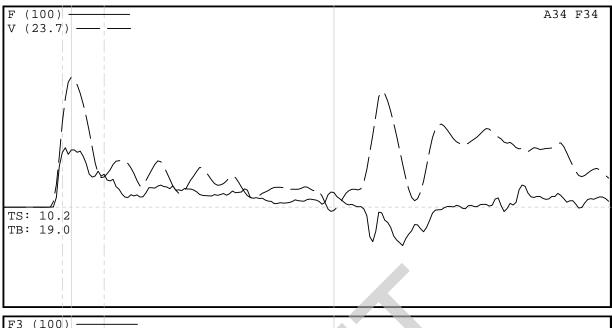
Time Summary

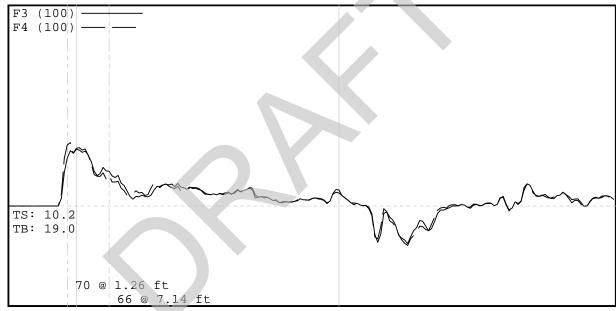
12:06:47 PM - 12:07:21 PM (6/21/2013) BN 1 - 14 Drive 34 seconds

MID BARATARIA CALIBRATION - BLUE FAILING TEST 3



BLUE FAILING TEST 3





Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: BLUE FAILING TEST 3 DESCR: SPT NRG MEAS. 3

OPERATOR: IAH

FILE: BLUE FAILING TEST 3.W01 6/21/2013 12:07:06 PM

Blow Number 7

Blow Number 7

Pile Properties

LE 37.00 ft AR 2.36 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 4.2 ksec/ft 2L/C 4.41 ms JC 0.35 [] LP 33.00 ft

Quantity Results

FMX 29 kips VMX 15.3 f/s DMX 1.47 in BPM 28.4 bpm EFV 0.27 k-ft EMX 0.27 k-ft ETR 77.1 (%) RX6 26 kips LTD 7.14 ft

Sensors

F3: [151 N3-1] 215.1 (1) F4: [151 N3-2] 216.74 (1) A3: [K1580] 355 mv/5000g's (1) A4: [K1578] 325 mv/5000g's (1) CLIP: OK

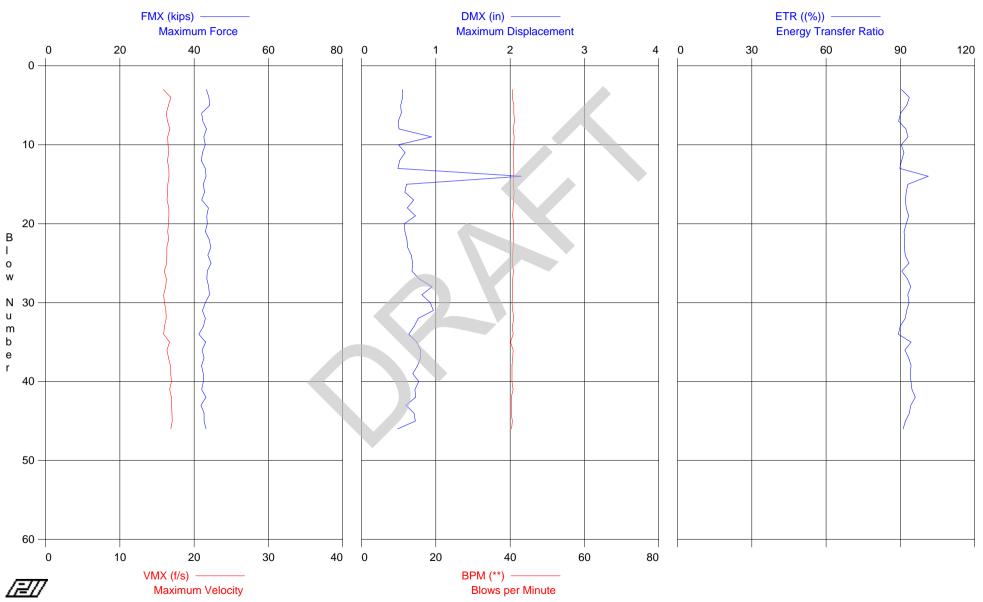
| MID BARATARIA CALIBRATION - SPT 32.33 TO 33.83 | |
|--|--|
| 00 100//14174 | |

| MID BARATARIA CALIBRATION - SPT 32.33 TO 33.83 | | | | | | | | SPT NRC | MEAS. 7 | |
|--|--------------|------|------|------|------|--------|--|---------------|-------------|--|
| OP: NICK MATA | | | | | | | Te | est date: 11- | -May-2013 | |
| AR: 1.32 in^2 | | | | | | | | SP: | 0.492 k/ft3 | |
| LE: 38.16 ft | | | | | | | | EM: 3 | 0,000 ksi | |
| WS: 16,807.9 f/s | | | | | | | | JC: | 0.35 | |
| FMX: Maximum Ford | e | | | | | EMX: N | lax Transferre | d Energy | | |
| VMX: Maximum Velo | city | | | | | ETR: E | nergy Transfe | er Ratio | | |
| DMX: Maximum Disp | lacement | | | | | RX6: N | RX6: Max Case Method Capacity (JC=0.6) | | | |
| BPM: Blows per Min | ute | | | | | LTD: L | LTD: Length to Damage | | | |
| EFV: Energy of FV | | | | | | | | | | |
| Statistics for entire file | e (44 blows) | | | | | | | | | |
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD | |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft | |
| Average | 43 | 16.5 | 0.71 | 40.7 | 0.32 | 0.32 | 92.5 | 18 | 17.80 | |
| Std. Dev. | 1 | 0.3 | 0.25 | 0.2 | 0.01 | 0.01 | 2.0 | 1 | 3.43 | |
| Maximum | 45 | 17.1 | 2.15 | 41.2 | 0.36 | 0.36 | 101.3 | 21 | 19.50 | |
| @ Blow# | 25 | 45 | 14 | 7 | 14 | 14 | 14 | 3 | 12 | |

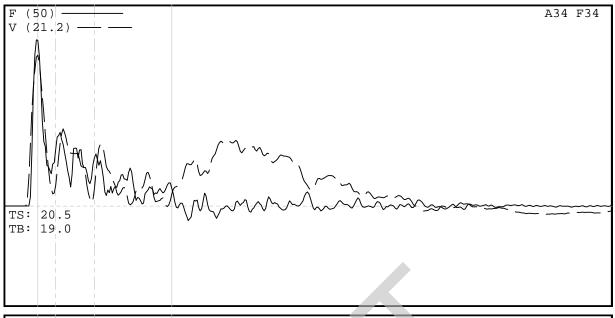
Time Summary

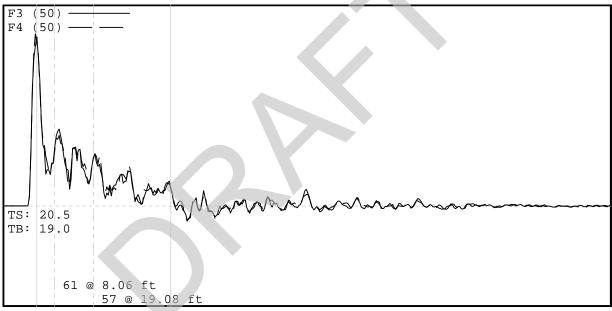
11:38:29 AM - 11:41:51 AM (5/11/2013) BN 1 - 46 Drive 3 minutes 22 seconds

MID BARATARIA CALIBRATION - SPT 32.33 TO 33.83



SPT 32.33 TO 33.83





Project Information

PROJECT: MID BARATARIA CALIBRATION PILE NAME: SPT 32.33 TO 33.83 DESCR: SPT NRG MEAS. 7 OPERATOR: NICK MATA FILE: SPT 32.33 TO 33.83.W01 5/11/2013 11:41:32 AM

Blow Number 34

Pile Properties

38.16 ft 1.32 in^2 AR ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.4 ksec/ft 2L/C 4.50 ms JC 0.35 [] LP 32.33 ft

Quantity Results

FMX 41 kips VMX 15.9 f/s DMX 0.64 in BPM 40.8 bpm EFV 0.31 k-ft EMX 0.31 k-ft ETR 89.1 (%) RX6 17 kips LTD 19.08 ft

Sensors

F3: [213BR1] 214.16 (1) F4: [213BR2] 216.06 (1) A3: [K1580] -355 mv/5000g's (1) A4: [K1578] -325 mv/5000g's (1) CLIP: OK MID BARATARIA CALIBRATION - 1_1 SPT NRG MEAS. 2

OP: IAH Test date: 13-May-2013 AR: 1.32 in^2 SP: 0.492 k/ft3 LE: 43.16 ft EM: 30,000 ksi WS: 16,807.9 f/s JC: 0.35

FMX: Maximum Force EMX: Max Transferred Energy VMX: Maximum Velocity

ETR: Energy Transfer Ratio
RX6: Max Case Method Capacity (JC=0.6) DMX: Maximum Displacement

BPM: Blows per Minute LTD: Length to Damage EFV: Energy of FV

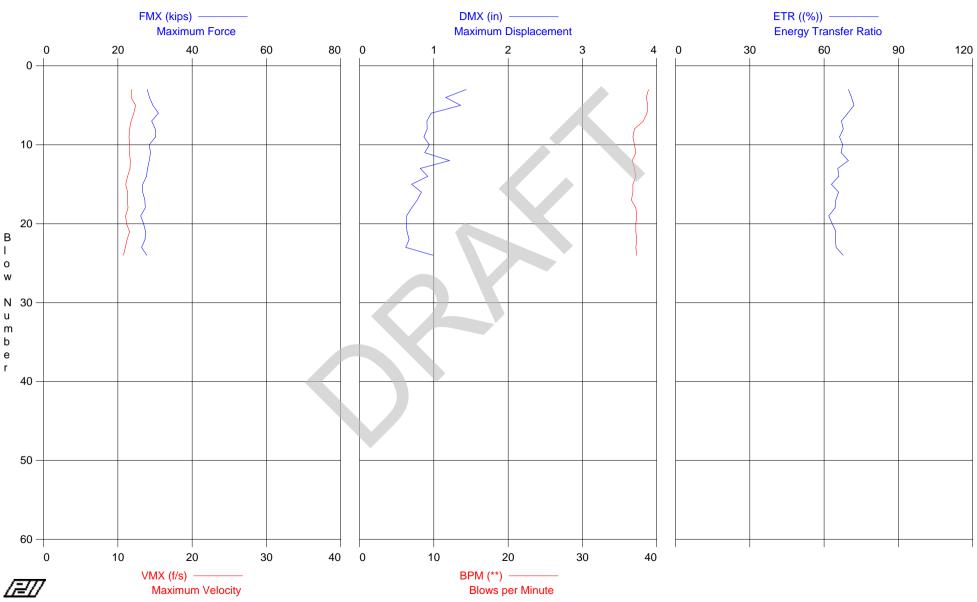
Statistics for entire file (22 blows) FMX VMX DMX BPM EFV EMX

ETR RX6 LTD f/s k-ft k-ft (%) kips ft Average 37.4 28 11.5 0.89 0.23 0.23 66.5 6 17.00 Std. Dev. 2 0.4 0.23 0.7 0.01 0.01 2.6 4.99 1 Maximum 31 12.4 1.43 23.03 38.9 0.25 0.25 72.1 12 @ Blow# 10 6 5 3 3 5 4

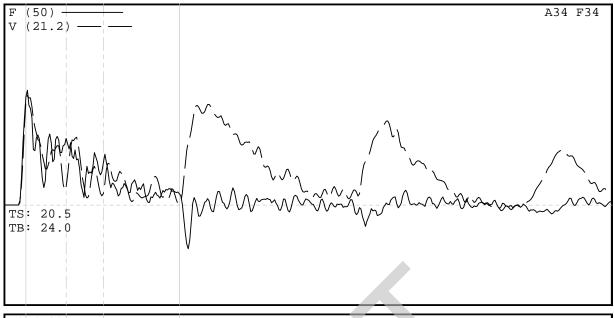
Time Summary

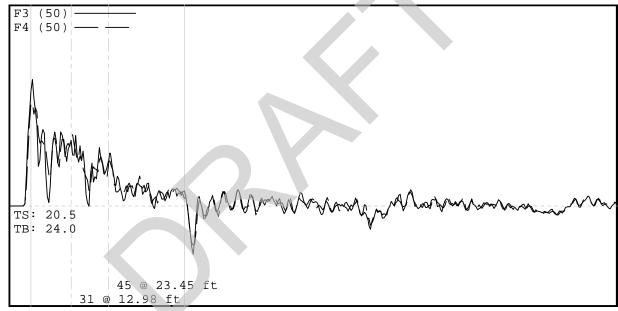
7:36:53 AM - 7:37:30 AM (5/13/2013) BN 1 - 24 Drive 37 seconds





1_1





Project Information

PROJECT: MID BARATARIA CALIBRATION

PILE NAME: 1_1

DESCR: SPT NRG MEAS. 2

OPERATOR: IAH FILE: 1_1.W01 5/13/2013 7:37:07 AM Blow Number 10

Pile Properties

LE 43.16 ft
AR 1.32 in^2
EM 30000 ksi
SP 0.492 k/ft3
WS 16807.9 f/s
EA/C 2.4 ksec/ft
2L/C 5.15 ms
JC 0.35 []

Quantity Results

FMX 28 kips VMX 11.6 f/s DMX 0.94 in BPM 37.0 bpm EFV 0.24 k-ft EMX 0.24 k-ft ETR 67.5 (%) RX6 12 kips LTD 12.98 ft

Sensors

F3: [213BR1] 214.16 (1) F4: [213BR2] 216.06 (1) A3: [K1580] -355 mv/5000g's (1) A4: [K1578] -325 mv/5000g's (1) CLIP: OK

Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 20-Jun-2013

| MID BARATARIA CALIBRATION - 1 | 1_2 |
|-------------------------------|-----|
| OD. IAII | |

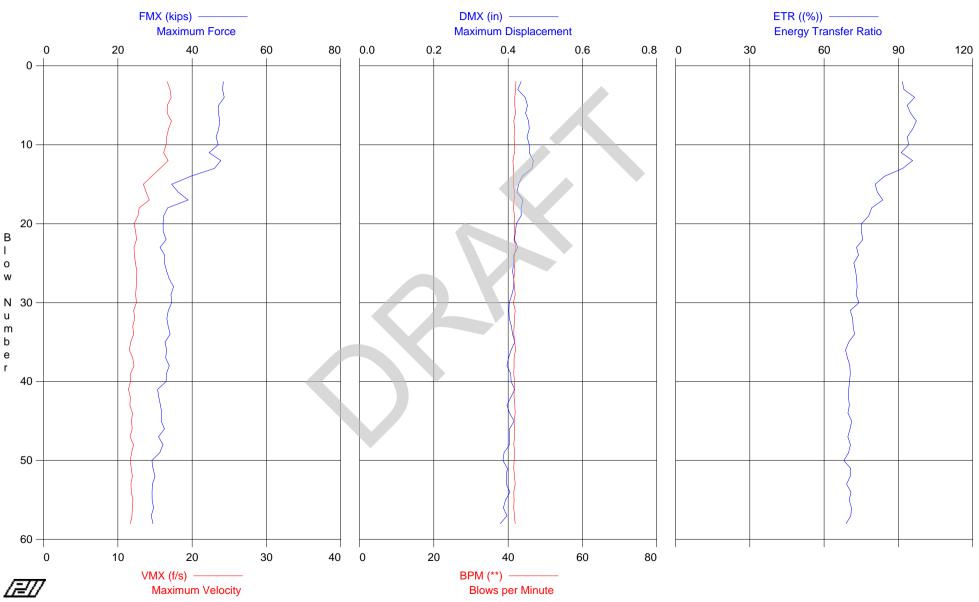
| MID BARATARIA CALIBRATION - 1_2 SPT | | | | | | | | SPT NR | G MEAS. 3 | | |
|-------------------------------------|-----------|------|------|------|------|---------|--|--------------|-------------|--|--|
| OP: IAH | | | | | | | Te | est date: 13 | -May-2013 | | |
| AR: 1.32 in^2 | | | | | | | | SP: | 0.492 k/ft3 | | |
| LE: 53.16 ft | | | | | | | | EM: 3 | 0,000 ksi | | |
| WS: 16,807.9 f/s | | | | | | | | JC: | 0.35 | | |
| FMX: Maximum Force | | | | | | EMX: M | ax Transferre | d Energy | | | |
| VMX: Maximum Veloci | ty | | | | | ETR: E | nergy Transfe | er Ratio | | | |
| DMX: Maximum Displa | cement | | | | | RX6: M | RX6: Max Case Method Capacity (JC=0.6) | | | | |
| BPM: Blows per Minute |) | | | | | LTD: Le | LTD: Length to Damage | | | | |
| EFV: Energy of FV | | | | | | | | | | | |
| Statistics for entire file (| 57 blows) | | | | | | | | | | |
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD | | |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft | | |
| Average | 36 | 13.2 | 0.42 | 41.7 | 0.27 | 0.27 | 77.1 | 15 | 13.26 | | |
| Std. Dev. | 6 | 1.9 | 0.02 | 0.2 | 0.03 | 0.03 | 9.5 | 2 | 1.35 | | |
| Maximum | 49 | 17.2 | 0.47 | 42.1 | 0.34 | 0.34 | 97.3 | 20 | 23.05 | | |
| @ Blow# | 4 | 7 | 12 | 2 | 7 | 7 | 7 | 7 | 25 | | |

Time Summary

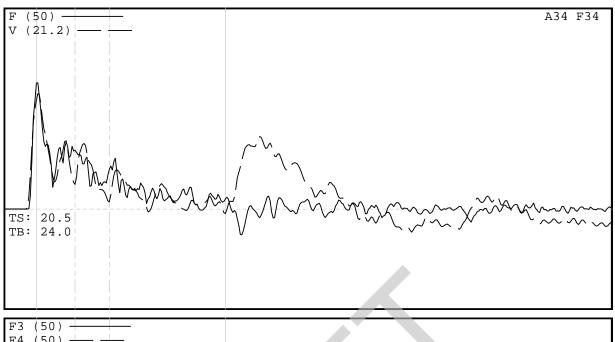
8:23:57 AM - 8:25:19 AM (5/13/2013) BN 1 - 58 Drive 1 minute 22 seconds

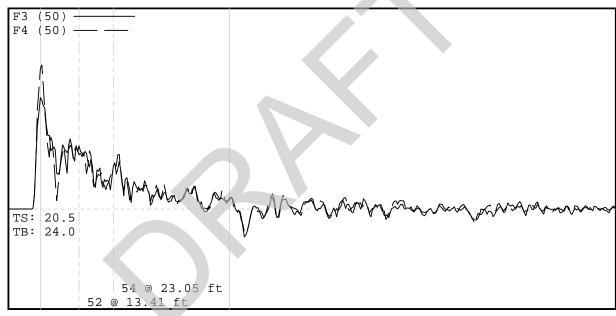
Test date: 13-May-2013

MID BARATARIA CALIBRATION - 1_2









Project Information

PROJECT: MID BARATARIA CALIBRATION

PILE NAME: 1_2

DESCR: SPT NRG MEAS. 3

OPERATOR: IAH FILE: 1_2.W01 5/13/2013 8:24:29 AM Blow Number 23

Pile Properties

LE 53.16 ft AR 1.32 in^2 ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.4 ksec/ft 2L/C 6.34 ms JC 0.35 [] LP 47.33 ft

Quantity Results

FMX 31 kips VMX 12.2 f/s DMX 0.43 in BPM 42.1 bpm EFV 0.26 k-ft EMX 0.26 k-ft ETR 73.1 (%) RX6 14 kips LTD 13.41 ft

Sensors

F3: [213BR1] 214.16 (1) F4: [213BR2] 216.06 (1) A3: [K1580] 355 mv/5000g's (1) A4: [K1578] 325 mv/5000g's (1) CLIP: OK

Page 1 of 1 PDIPLOT Ver. 2012.2 - Printed: 20-Jun-2013

| /IID BARATARIA CALIBRATION - 1_3 | SPT NRG MEAS. 4 |
|----------------------------------|------------------------|
| DP: IAH | Test date: 13-May-2013 |

| OP: IAH | Test date: 13-May-2013 |
|--------------------|-----------------------------|
| AR: 1.32 in^2 | SP: 0.492 k/ft3 |
| LE: 56.16 ft | EM: 30,000 ksi |
| WS: 16,807.9 f/s | JC: 0.35 |
| FMX: Maximum Force | FMX: Max Transferred Energy |

| FIVIX: | Maximum Force | FIVIX: | Max Transferred Energy |
|--------|----------------------|--------|-----------------------------------|
| VMX: | Maximum Velocity | ETR: | Energy Transfer Ratio |
| DMX: | Maximum Displacement | RX6: | Max Case Method Capacity (JC=0.6) |

LTD: Length to Damage

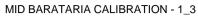
BPM: Blows per Minute EFV: Energy of FV

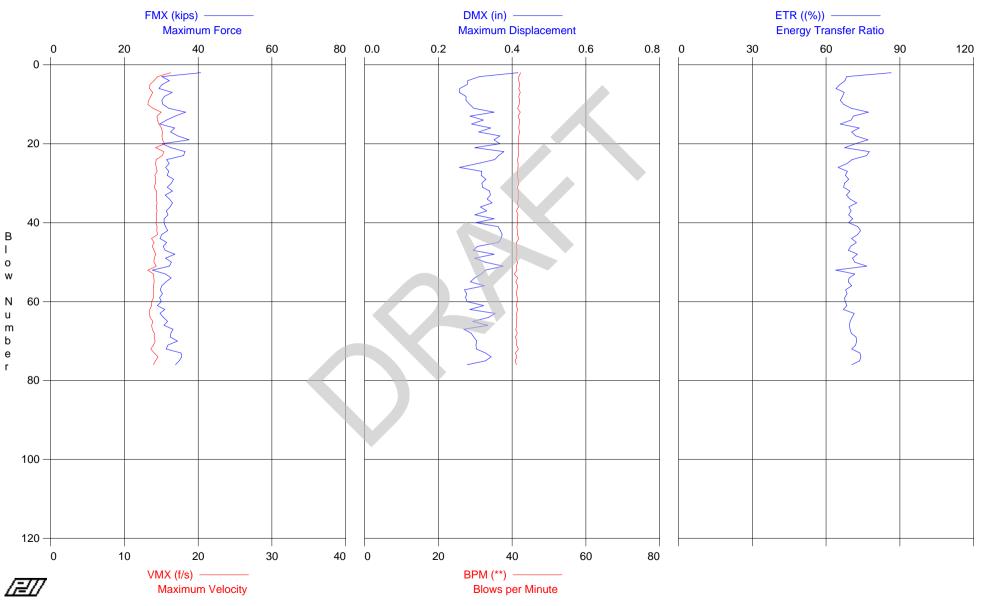
| Statistics for entire fil | e (75 blows) | | | | | | | | |
|---------------------------|--------------|------|------|------|------|------|------|------|-------|
| | FMX | VMX | DMX | BPM | EFV | EMX | ETR | RX6 | LTD |
| | kips | f/s | in | ** | k-ft | k-ft | (%) | kips | ft |
| Average | 32 | 14.2 | 0.32 | 41.5 | 0.25 | 0.25 | 70.4 | 13 | 16.69 |
| Std. Dev. | 2 | 0.5 | 0.03 | 0.3 | 0.01 | 0.01 | 3.5 | 1 | 1.22 |
| Maximum | 41 | 16.3 | 0.42 | 42.3 | 0.30 | 0.30 | 86.5 | 15 | 17.60 |
| @ Blow# | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 71 | 31 |

Time Summary

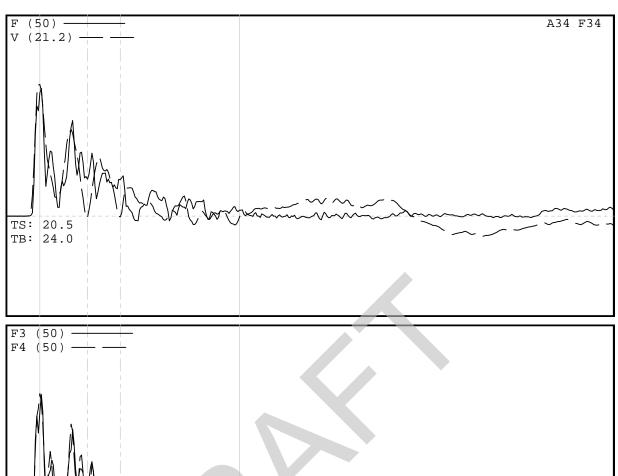
9:06:23 AM - 9:08:11 AM (5/13/2013) BN 1 - 76 Drive 1 minute 48 seconds

Test date: 13-May-2013









Project Information

PROJECT: MID BARATARIA CALIBRATION

40 @ 15.93 ft

49 @ 25.15 ft

PILE NAME: 1_3

20.5

24.0

TS:

TB:

DESCR: SPT NRG MEAS. 4

OPERATOR: IAH FILE: 1_3.W01 5/13/2013 9:07:55 AM Blow Number 65

Pile Properties

LE 56.16 ft 1.32 in^2 AR ΕM 30000 ksi SP 0.492 k/ft3 WS 16807.9 f/s EA/C 2.4 ksec/ft 2L/C 6.70 ms JC 0.35 [] LP 52.33 ft

Quantity Results

FMX 32 kips VMX 13.9 f/s DMX 0.29 in BPM 41.1 bpm EFV 0.24 k-ft EMX 0.24 k-ft ETR 69.7 (%) RX6 14 kips LTD 15.93 ft

Sensors

F3: [213BR1] 214.16 (1) F4: [213BR2] 216.06 (1) A3: [K1580] 355 mv/5000g's (1) A4: [K1578] 325 mv/5000g's (1) CLIP: OK